U.S. Department of Transportation United States Coast Guard



Merchant Marine Deck Examination Reference Material

OPERATING MANUAL FOR COASTAL DRILLER

PLEASE NOTE

This manual has been prepared solely for use with MODU license examinations. The policies and procedures outlined should not be used as a guide for the operation of any specific unit. Use only the policies and procedures outlined in the manual developed specifically for the unit. Because this manual is incomplete, it should *not* be used as a model for preparing MODU operating manuals for compliance with 46 CFR 109.121.

Aug 1989

This publication contains information to be used in examinations for merchant marine licenses and documents.

COMDTPUB P16721.30

U.S. Department of Transportation

United States Coast Guard



Commandant (G-MVP) United States Coast Guard

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COMDTPUB P16721.30

2 NOV 1989

COMMANDANT PUBLICATION P16721.30

- Subj: Merchant Marine Deck Examination Reference Book, OPERATING MANUAL FOR COASTAL DRILLER.
- 1. <u>PURPOSE</u>. This publication contains reference material that may be needed by an applicant during an examination for a merchant marine deck license.

2. DISCUSSION.

- a. Applicants for merchant marine deck licenses taking an examination to determine their professional qualifications may be required to answer examination questions which are based on the material in this publication.
- b. The Coast Guard has converted to a computerized random generation system for creating examination modules. To streamline the process of creating module test booklets, where possible, the reference material needed to answer exam questions has been incorporated in Deck Examinations Reference Books. This allows applicants to view both the exam question and the reference material at the same time.
- c. Copies of this publication will be provided by the Regional Examination Centers (RECs) when applicants take an examination. This publication is available to the general public but only copies provided by the RECs may be used when completing an examination.
- d. The August 1989 edition of this publication contains all material required by questions in the question bank as of August 1989.

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3. <u>PROCEDURE</u>. This publication will be made available to applicants taking a deck merchant marine examination. Applicants who have purchased copies of this publication from the Government Printing Office (GPO) may not use their personal copies during examinations. Each REC is to allow only the REC copies of this publication to be used in the exam room. The covers of this publication held by the RECs will be gray; the covers of this publication available to the public through GPO will be yellow.

4. ORDERING INFORMATION.

- a. Regional examination centers will be provided with an initial supply of this publication. Replacement and additional copies are available from Commandant (G-MVP-5), FTS 267-2705.
- b. The public and other Coast Guard units may order copies of this publication from the GPO at the following address:

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INSTRUCTIONS

1. Some of the questions in the deck examination booklets require the use of mobile offshore drilling unit (MODU) reference material to answer the question. All of the material necessary to these questions is contained in the appropriate Merchant Marine Deck Examination Reference Book.

2. If a question requires the use of mobile offshore drilling unit reference materials, the stem of the question will make reference to the MODU in question. For example, if the question in your examination booklet is, "The center of flotation for the Coastal Driller is located at the geometric center of the ______, you must use The Merchant Marine Deck Examination Reference Book, OPERATING MANUAL FOR COASTAL DRILLER to answer the question.

3. The Merchant Marine Deck Examination Reference Book, OPERATING MANUAL FOR COASTAL DRILLER, has been prepared solely for use with MODU license examinations. The policies and procedures outlined should not be used as a guide for the operation of any specific unit. Use only the policies and procedures outlined in the manual developed specifically for the unit. Because this manual is incomplete it should not be used as a model for preparing MODU operating manuals for compliance with 46 CFR 109.121.

4. Applicants taking an examination who wish to make a comment or protest concerning any material in this publication should complete a Comment/Protest form for the question involved and give it to the examiner.

5. Individuals not taking an examination who wish to make a comment on any material in this publication should send a written comment, citing this publication and the appropriate page, and paragraph or illustration commented on, to:

Commandant (G-MVP-5) U.S. Coast Guard OPERATING MANUAL FOR COASTAL DRILLER 2100 Second Street SW Washington, DC 20593-0001

All written comments submitted by the general public will be reviewed prior to revising this publication. A heavy workload precludes the Merchant Marine Examination Branch from discussing comments over the telephone or responding to written comments. Your comments are welcomed and you will receive a letter or postcard indicating your comments were received. The assistance of the following companies in the development of this manual is gratefully acknowledged:

Marathon LeTourneau Marine Company Penrod Drilling Corporation

Prepared as a part of Coast Guard contract DTCG23-88-C-10082 by Houston Marine Training Services

TABLE OF CONTENTS

CHAPTER 1 GENERAL DESCRIPTION

			PAGE			
1.	Gene	1-1				
2.	Person-in-Charge					
3.	Princ	cipal Dimensions	1-2			
4.	Liqu	id and Bulk Capacities	1-3			
5.	Desi	gn Deck Loading	1-3			
6.	Envi	ronmental Considerations	1-3			
7.	Weig	ght and Load Definitions	1-3			
	a.	Lightship Weight	1-3			
	b.	Variable Load	1-4			
	c.	Preload	1-4			
	d.	Drilling Loads	1-4			
8.	Ligh	1-5				
	a.	Summary of Lightweight Condition	1-5			
	b.	Hull, Basic Load, and Stationary Fixed Load	1-5			
	c.	Cantilever Beams and Subbase	1-6			
	d.	Substructure, Derrick, & Drill Floor	1-6			
	e.	Legs and Spud Cans	1-6			
9.	Char	nges to Lightweight	1-6			
10.	Max	imum Operating Variable Loads	1-7			
11.	Prelo	bad Requirements	1-7			
12.	Spuc	1 Can Reactions	1-7			
13.	Elev	ating System Load Capacities	1-8			
14.	Drill	ing Component Capacities	1-8			
15.	Snov	w and Ice	1-8			
16.	Mari	ine Growth Accumulation	1-9			
17.	Tests	s and Inspections	1-9			
18.	Refe	rence Planes, Units, and Precision Standards	1-9			

CHAPTER 2 AFLOAT OPERATIONS

1.	Stability Criteria	2-1
2.	Preparing the Unit for Afloat Operations	2-1
3.	Maintaining Watertight Integrity	2-1

i

Ρ	A	G	Ε	
		~	-	

4.	Load	oad Form						
5.	Operational Instructions - Lowering Hull and Refloating							
	a.	Checklist for Going Off Location	2-3					
	b.	Lowering the Hull	2-3					
	C.	Jetting Out	2-4					
6.	Operational Instructions - Afloat							
	a.	Transit Types	2-5					
		(1) Field Transit	2-5					
		(2) Ocean Transit	2-5					
		(3) Floating Conditions	2-6					
	b.	b. Limits of Service Afloat						
	c.	Operational Recommendations - General Afloat	2-7					
	d.	Operational Recommendations - Severe Storm	2-7					
		(Afloat)						
	e.	Changing Modes of Operation Afloat	2-8					
7.	Emergency Procedures for Unexpected Inclination							
	a.	Possible Causes of Unexpected Inclination	2-9					
	b.	Corrective Actions - Inclination Rapidly Increasing	2-9					
	c. Corrective Actions - Inclination Slowly Increasing							
	d.	d. Corrective Actions - Inclination Constant						
8.	8. Bilge System							
	-							

CHAPTER 3 ELEVATED OPERATIONS

1.	Prepa	aration for Elevating					
	a.	a. Geotechnical Information					
	b.	Safe Motion for Going-on Location	3-1				
	c.	Checklist for Elevating	3-2				
2.	Preloading						
	a.	Preloading Procedures	3-3				
	b.	Elevating Procedures	3-4				
3.	Eleva	ated Operations	3-5				
4.	Leg I	Leg Reaction					
5.	Operational Instructions - Normal Drilling						
	a.	General Elevated Instructions	3-6				
	b.	Allowable Wind and Wave Charts	3-7				
6.	Oper	ational Instructions - Severe Storm (Elevated)	3-8				
7.	Limit	ts of Service - Elevated	3-9				
8.	Emergency Information 3-10						
9.	Prepa	aring the Unit for Evacuation	3-11				

CHAPTER 4 STABILITY CALCULATIONS

1.	Load	d Form Organization	4-1			
	a.	Sheet 1	4-2			
	b.	Sheet 2	4-3			
	c.	Sheet 3	4-3			
2.	Afloat Stability					
	a.	Hydrostatic Data	4-4			
	b.	Stability Data	4-5			
	с.	Trim and List	4-6			
	d.	Drafts	4-6			
3.	Leg	Reaction Calculation	4-7			
4.	Prel	oad Distribution Calculation	4-8			
5.	Sam	ple Load Forms	4-11			
	a.	Rig Move	4-13			
	b.	Preloading	4-17			
	с.	Normal Drilling	4-21			
	d.	Elevated Severe Storm	4-25			

CHAPTER 5 OPERATING DATA

1.	Hydrostatic Properties	5-1
2.	Maximum Allowable KG	5-6
3.	Design Limits of Legs (Afloat)	5-7
4.	Safe Motion for Going on Location	5-8
5.	Allowable Wind and Wave	5-9
6.	Limits of Service	5-21
7.	Cantilever Beam Loading	5-22
8.	Changes to Lightweight	5-23

Charts, Tables, and Figures

	 ۰.	\sim	
۲			-
		~	

Table: Hydrostatic Properties	5-4
Graph: Maximum Allowable KG	5-6
Graph: Design Limits of Legs (Afloat)	5-7
Graph: Safe Platform Roll and Pitch for Going-On Location	5-8
Graph: Allowable Wind and Wave During Drilling	5-9
Table: Limits of Service	5-21
Table: Cantilever Beam Loading Chart	5-22
Table: Coastal Driller - Changes to Lightweight	5-23
Form: Leg Reaction Calculation	5-24
Form: Preload Calculation Sheet	5-25
Fig.1: Side View - Coastal Driller	5-26
Fig.2: Plan View - Coastal Driller	5-27
Fig.3: Inner Bottom Layout - Bilge Suction Piping	5-28
Fig.4: Machinery Deck Layout	5-29

CHAPTER 6 TANK CAPACITY TABLES

1.	Densities	6-1
2.	Reference Axis and Signs	6-1
3.	Weight of Mud to be Added to Load Form	6-1
4.	Tank Tables Summary	6-2
5.	Tank Tables (Numerical Order)	

Service	
Drill Water	6-3
Preload	6-4
Preload	6-5
Potable Water	6-6
Drill Water	6-7
Preload	6-8
Preload	6-9
Drill Water	6-10
Diesel Fuel	6-11
Diesel Fuel	6-12
	Service Drill Water Preload Potable Water Drill Water Preload Preload Drill Water Diesel Fuel Diesel Fuel

		PAGE
15 or 16	Preload	6-15
17	Drill Water	6-16
18	Drill Water	6-17
19	Diesel Fuel	6-18
20	Diesel Fuel	6-19
21A	Preload	6-20
21B	Preload	6-21
22A	Preload	6-22
22B	Preload	6-23
23 or 24	Drill Water	6-24
25 or 26	Drill Water	6-25
28	Preload	6-26
29	Preload	6-27
31	Dirty Oil	6-28
Skim Tank		6-29
MudPit 1S		6-30
MudPit 2S		6-31
MudPit 3P		6-32
MudPit 4P		
Slugging Pit		

V

CHAPTER 1 - GENERAL DESCRIPTION

1. GENERAL INFORMATION

The Coastal Driller is a non-propelled, self-elevating mobile offshore drilling unit inspected and certified by the U.S. Coast Guard and classed by American Bureau of Shipping as

1A1 SELF ELEVATING UNIT

The unit is designed for operation in water depths of up to 250 feet. The unit is also designed for ocean transit, afloat on its own hull with its legs intact and fully raised so that the spud can tip is 12.38 feet below the bottom of the hull.

The unit consists of a welded steel hull of a modified triangular shape in plan view. It is equipped with three truss-type triangular legs, each fitted with a spud-can type footing at the lower ends. The legs can be lowered to the ocean floor after which the hull can be elevated above the sea surface. The legs are elevated and lowered by means of a rack and pinion jacking system. The bow leg is on the centerline at the forward end of the unit.

Crew accommodations for 72 men are located in the four-level quarters structure on the main deck just aft of the bow leg. The galley and mess area are located on the first level. Also on the first level is a six-man treatment room. Two recreation rooms, laundry, and eleven four-man rooms are located on the second level. The administrative offices, six two-man rooms, and four four-man rooms are located on the third level. The control room is located on the fourth level.

The hull houses the engine room, auxiliary machinery room, mud pump room, sack storage room, workshop, drill tool stores, and tanks for liquids. The helideck, a polygon circumscribed in a 65 ft. diameter circle forward of the bow leg, is designed for a Sikorsky S-61 helicopter.

Just aft of the crew accommodations on the main deck are two longitudinal cantilever beams. Each is located 25 feet off the centerline port and starboard. The drilling structure is mounted on the extreme after end of the beams. The beams can be skidded fore and aft 68.0 feet to place the rotary as much as 40.0 feet aft of the stern. The drilling structure can then skidded as much as 10.0 feet port or starboard.

2. PERSON-IN-CHARGE

The person designated by the Contractor as the Offshore Installation Manager (OIM) has the responsibility for the unit. Normally, when operating in the elevated mode, that person is the senior toolpusher. While lowering the hull in preparation for a move, while underway, and while elevating and preloading at a new location, a person holding a license as OIM Bottom Bearing Unit Underway must be designated as the person-in-charge.

3. PRINCIPAL DIMENSIONS

Length overall (including helideck)	277.30	feet
Length of hull	207.33	feet
Breadth of hull overall	176.00	feet
Depth of hull	20.00	feet
Load line displacement	14,158.31	kips
Load line draft	10'10.5"	
Draft mark locations		
Forward marks (38.12 ft AF0, 37.69 ft off CL)		
Aft marks (160.17 ft AF0, 88.0 ft off CL)		
Overall length of legs	360.33	feet
Longitudinal leg spacing	121.67	feet
Transverse leg spacing	120.00	feet
Minimum leg spacing	107.63	feet
Leg projection below hull		
Minimum Tip of Can (TOC) position	1.20	feet
Severe storm TOC	60.50	feet
Depth of cans (including tip)	21.00	feet
Diameter of cans (across flats)	40.00	feet
Projected footing area	1,235.00	sq ft
Length of raw water tower	127.00	feet
Drill floor: transverse travel	±10.00	feet
Cantilever substructure:		
Total longitudinal travel	68.33	feet
Maximum distance rotary aft of transom	40.00	feet

4. LIQUID AND BULK CAPACITIES

Fuel oil	2,276 bbls
Potable water	983 bbls
Drill water	6,631 bbls
Mud Pits	1,320 bbls
P-Tanks	7,700 cuft
Preload	8,708 kips

5. DESIGN DECK LOADING

Main deck	500 psf
Machinery deck	500 psf
Quarters deck & walkways	90 psf
Drill floor	
Within derrick b	base 500 psf
Outside derrick	base 270 psf
Cantilever pipe rack	270 psf
Pipe Rack Area +	500 kips total
Individual Pipe Rack Beam	5 kips per linear foot
+ Pipe to be uniformly dist	tributed
Drill Package Weight	1471.2 kips
Heliport designed for Sikor	sky S-61
Overall length:	72.9 ft (22.2 m)
Rotor size:	62.0 ft (18.9 m)

6. ENVIRONMENTAL CONSIDERATIONS

Heliport Size (across flats)

Gross Weight:

This unit was designed with the following environmental considerations:

20.5 tons (2,298 kg)

65.0 ft (19.8 m)

Temperature:		
Atmo	ospheric	+ 10°F (-12.2°C)
Wate	er	+ 28°F (- 2.2°C)
Snow/ice		Onboard accumulations must
		be removed as soon as possible.

7. a. Lightweight

The lightweight is the condition of the unit before loading cargo, fuel, water, or stores. For the Coastal Driller, the lightweight consists of the basic hull weight and the fixed weight. The fixed weight is that which is permanently attached to the unit, which includes a portion that is stationary and a portion that can be moved.

The basic hull weight consists of the hull steel and items necessary to maintain the unit in the afloat condition and lower the unit on the legs with the exception of the electric power source.

Items of basic load include the legs, spud cans, gear units, preload piping and eductor piping, control panels and wiring for the elevating systems of the legs, bilge piping, tank vents and sounding tubes, basic lighting in the hull, aids to navigation, cleats, bollards, fairleads, towing brackets, manholes, handrails, ladders, water-tight doors, basic hull painting, mud pit structure, and similar equipment.

Fixed loads consists of equipment more or less continuously attached to the unit. Items of fixed load include cranes, rig skidders, cantilever beams and substructure, helideck, winches, quarters, foundation, bulk mud and cement tanks, drilling machinery, derrick, engines and generators, control panels, pumps, degasser, shale shaker, cementing and logging unit, drill floor equipment, sea water tower and pumps and similar equipment.

b. Variable load

Variable loads are those items that are expendable, readily removable or consumable during drilling operations. They include such items as active mud, bulk mud, cement, chemicals, fuel oil, potable water, drill water, lube oil, casing, drill pipe, drill collars, spare parts, tools, stores, hotel supplies and weight of persons and their effects on board.

c. Preload

Preload is sea water temporarily pumped into tanks during the preloading operation to simulate the increased vertical loading imposed by the environmental forces. After the soil has stabilized following the preloading operation, the sea water is dumped. Any water remaining in the preload tanks must be either removed or its weight and center of gravity locations added to the variable loads.

d. Drilling Loads

Drilling loads are the combined loads arising from the hook, rotary, setback, and conductor tension loads. In the drilling mode, the drilling loads are not considered as part of the variable load of the unit. In the elevated severe storm condition, all drilling loads must be treated as variable loads. When changing from the drilling mode to the severe storm mode, setback must be returned to the pipe racks, and remaining hook loads, rotary, or conductor tension must be accounted for as part of the variable load.

Hook load is the force acting on the hook of the derrick. It includes the weight of the drill string.

Rotary load is the weight of the tubulars hung off in the rotary.

Setback is the weight of tubulars stored in the derrick.

Conductor tension is the vertical tension on the cantilever structure required to support the Conductor/Drive Pipe and BOP.

8. LIGHTWEIGHT AND COMPONENT WEIGHTS

The following describes the weight and the center of gravity locations of the basic hull and stationary load, cantilever beams and subbase, substructure and drill floor, and the legs and spud cans. Weights are measured in kips. LCG is located aft of frame zero (AF0); TCG is starboard (+) or port (-) of the hull centerline; and VCG is measured above (+) the hull baseline. See page 1-9 for a description of the coordinate system used with the Coastal Driller.

a. Summary of Lightweight Condition

Lightweight includes the effect of the three legs (360.33 feet), cantilever substructure, and the drill floor. In the lightweight configuration the spud can tips are located 12.38 feet below the hull baseline with the spud cans free-flooding. The cantilever beam is in the full forward position, with the centerline of the rotary 179.0 feet AF0 and on the hull centerline. The raw water tower is in the full up position and the cranes are in the stowed position.

The following lightweight conditions are based on the inclining experiment and deadweight survey report dated 15 October 1982:

Displacement	11,777.18 kips
LCG (AF0)	120.59 ft
TCG (Starboard of CL)	1.19 ft
VCG (Above hull baseline)	51.88 ft

b.

c.

Hull, Basic Load, and Stationary Fixed Load

Weight	7,068.86 kips
LCG (Measured AF0)	111.35 ft
TCG (Starboard of CL)	2.17 ft
VCG (Above BL)	19.54 ft

Cantilever Beams and Subbase

Weight	870.00 kips
LCG (Normal stowed position)	and the second
Measured AF0	157.19 ft
Forward of rotary	21.81 ft
TCG (Port of CL)	- 1.75 ft
VCG (Above baseline)	32.85 ft

d.

Substructure, Derrick, & Drill Floor

Weight	580.00 kips
LCG (Normal stowed position)	
Measured AF0	184.72 ft
Aft of rotary	5.72 ft
TCG (Starboard of CL)	+ 0.38 ft
VCG (Above baseline)	70.23 ft

e. Legs and Spud Cans

Weight	3,258.31 kips	
VCG (Above tip of can, TOC)	136.24 ft	

The individual legs are located as follows:

	LCG	TCG
Bow	38.33	0.0
Stbd	160.0	+ 60.0
Port	160.0	- 60.0
Geometric Cer	ter 119.44	0.0

9. CHANGES TO LIGHTWEIGHT

Alterations in weight and/or center of gravity location for structure or installed equipment must be kept by the OIM in a permanent record. These changes are to be treated as a variable load until a formal change to lightweight has been approved by the U.S.C.G. and ABS. The most recent weight and center of gravity location from the permanent record shall be used in the daily calculations in the load form.

WARNING

Increases in lightweight could cause overloading which could overstress the structure and/or raise the unit's KG and reduce its stability.

Changes to lightweight for the Coastal Driller which have taken place since the original inclining experiment (10/15/82) are shown in the formal record: Changes to Lightweight. See page 5-23.

The weights and moments shown in the record will be treated as a variable load until a change to lightship has been approved.

10. MAXIMUM OPERATING VARIABLE LOADS

The weight limit on variable loading is:

Afloat	2,381 kips
Elevating & Preload	2,381 kips
Elevated operating	3,381 kips
Severe storm	2,381 kips

11. PRELOAD REQUIREMENTS

The capacity of the unit's preload tanks (8,708 kips) is greater than the required preload. This excess capability permits additional preload when the variable loads onboard are less than the maximum of 2,381 kips during elevating and preloading.

12. SPUD CAN REACTIONS

When operating (drilling), the total loading on the legs, including static and environmental loading is acceptable provided the unit is preloaded according to the instructions in Chapter 3, and provided the maximum leg reactions shown in the Allowable Wind and Wave charts during drilling, are not exceeded. In a severe storm the additional environmental loading may cause soil failures if the procedures in Chapter 3 are not followed. In any case, the static loading on each of the legs must be *at least* 7,099 kips on each leg for preloading. In fact, it is better to go over 7,099 kips rather than under, as an extra 200 kips is allowed, distributed with up to 100 kips extra on a leg.

For the elevated storm condition, the maximum static loading is 4,720 kips on each leg. During drilling, the loading must be limited in accordance with the allowable wind and wave charts in Section 5.

13. ELEVATING SYSTEM LOAD CAPACITIES

The elevating system is normally limited to 14,400 kips. This means that normally the unit can be elevated with full variables and some preload on onboard, provided that the limit of 14,400 kips is not exceeded.

In an emergency, the unit is capable of elevating with a loading of 5,760 kips per leg (17,280 kips for the unit).

Elevating capacity	14,400.0 kips	
Holding capacity		
Drilling	17,280.0 kips	
Severe storm	14,400.0 kips	

14. DRILLING COMPONENT CAPACITIES

The cantilever and associated structures are designed to the following structural limits.

Setback load	450 kips		
Rotary load	750 kips		
Hook load	1,000 kips		
Combined drilling load	1,000 kips		
Cantilever pipe rack	500 kips		

Depending on the placement of the rotary when in the drilling mode, the allowable combined drilling load consisting of the combined hook, rotary, setback, and conductor tension shall not exceed the values shown on page 5-22.

15. SNOW AND ICE

Accumulations of snow or ice cause increased weight loads and increased environmental loads from wind, wave, and currents. Both may combine to overload the legs, elevating system, helideck, derrick, and cantilever. Snow and icing conditions constitute a safety hazard during which the entire unit should be checked regularly for accumulations. Should accumulations be found, it must be removed immediately. The unit is not ice strengthened; therefore, it should not be operated in areas where significant amounts of solid or flow ice are present.

16. MARINE GROWTH ACCUMULATION

Marine growth may accumulate on the legs when the unit is in service. The effect is twofold. Weight and the environmental forces due to waves and current increase. During transits the legs should be examined, and the marine growth removed as necessary.

17. TESTS AND INSPECTIONS

Emergency, lifesaving, and firefighting systems are to be tested and inspected in accordance with Title 46 of the Code of Federal Regulations, Subchapter I-A.

18. REFERENCE PLANES, UNITS, AND PRECISION STANDARDS

Reference Planes

Distances aboard the rig are measured from the following reference planes:

Vertical measurements are made from an horizontal reference plane, or baseline, passing through the underside of the hull. Distances measured vertically upward are considered positive; distances below the hull are treated as negative quantities.

Longitudinal measurements are made from a transverse vertical plane passing through Frame zero at the bow. Distances aft of frame zero (AF0) are considered positive. Those forward of frame zero (FF0) are considered negative.

Transverse measurements are made from a vertical plane passing through the longitudinal centerline of the vessel. Distances to starboard are considered as positive quantities. Those to port are considered as negative quantities.

Units

Weights (Loads) Distances Moments

kips (1,000 lbs) feet ft-kips Precision should be kept to the following standards:

Distances	Two dea		
Weights	One dec		
Moments	Nearest		

wo decimal places one decimal place learest whole number

When "rounding", use the next higher number if the digit one place beyond the above standards is 5 or more. Use the next lower number if the digit is 4 or smaller. For example, if the distance is computed to be 52.485 feet, round up to 52.49 feet. If the weight is calculated to be 102.94 kips, use 102.9 kips. If the moments are computed to be 3,456.5 ft-kips, use 3,457 ft-kips.

CHAPTER 2 - AFLOAT OPERATIONS

This chapter provides guidance for afloat operations and for preparing the Coastal Driller for afloat operation.

1. STABILITY CRITERIA

The hull has adequate reserve intact stability for winds up to 70 knots, and up to 100 knots if the legs are lowered so that the tip of the spud cans (TOC) is 60.5 feet below the baseline (keel).

In calm seas and winds to 50 knots, the unit has sufficient reserve stability to withstand flooding due to damage of any one watertight compartment. Damage is considered to be the result of penetration of the hull from the side or bottom. It is assumed that the penetration depth is limited to five feet (1.5 meters), and that watertight closures are secured.

The ability to meet the intact and damage stability criteria depends on maintaining a watertight environment, displacement less than the maximum of 14,158 kips, corrected vertical center of gravity less than the maximum allowed, and a level attitude.

2. PREPARING THE UNIT FOR AFLOAT OPERATIONS

The preparations required to make the unit seaworthy before commencing a wet tow are the same regardless of whether the unit is initially elevated, on a dry tow vessel, or afloat at dockside. These preparations consist of securing all openings to maintain the unit's watertight envelope, properly stowing all loads to prevent their shifting, and using a load form to determine the unit's draft, trim, list, and stability. Additional steps are required when refloating the unit from the elevated condition.

3. MAINTAINING WATERTIGHT INTEGRITY

The following steps are used to help maintain watertight integrity:

a. Close and secure all watertight doors, companionways, cargo hatches, preload hatches, man-holes, ventilation closures, through-bulkhead vents, deadlights, and other watertight fixtures.

b. Install blanks, cap or close all valves for preload dumps, equalizers, throughhull drains, mud pit dumps, fill lines, and sounding tubes.

WARNING

The mud return line must be blanked off or closed for all afloat operations. Sand trap drains must be opened to prevent water flowing back to the mud pits.

- c. Test the bilge pumps. Then close all sump and bilge manifold valves.
- d. Close the gear unit motor covers when not in use to reduce environmental damage to electrical equipment.
- e. Stow and secure all movable equipment, bulk material, stores, spare parts, tubulars, and other loose articles to prevent a shift in the loading.

4. LOAD FORM

The load form is used to determine the unit's displacement and the three components of the center of gravity location (LCG, TCG, and VCG). When floating, it is necessary to ensure that the load line displacement and maximum allowable KG are not exceeded. LCG and TCG are used to determine the proper load distribution for a level attitude.

The load form is to be completed daily. Additionally, a load form should be completed before making major changes in loading, and prior to lowering the hull into the water. The general procedures for completing the form are described in Chapter 4.

5. OPERATIONAL INSTRUCTIONS - LOWERING THE HULL AND REFLOATING

Lowering the hull and refloating should be done in favorable weather conditions, with wave heights less than five feet.

a. Checklist for going off location

- (1) Prepare the unit for afloat condition.
- (2) Check that the length of the raw water tower and the water depth is such that the tower does not contact the sea bottom as the hull is lowered. This is especially important when jacking down in shallow water.
- (3) Prepare a load form for the afloat condition. Determine expected floating stability, draft, list, and trim.
- (4) Check that the motor brake release and gear trains are operable.
- (5) Check that weather is acceptable for the time period of lowering the hull, transitting, and elevating at the new location. In particular wave heights as measured from trough to crest should not exceed 5'.

b. Lowering the hull

- (1) Start the generators and notify all personnel to report to their proper stations for jacking.
- (2) Energize the jacking console and note the level reading on the indicators.
- (3) Open all elevating motor covers during jacking to improve cooling of the motors.
- (4) Advise all personnel that jacking is about to begin. Instruct the leg observers to lubricate the gear mechanisms, and to monitor the legs as they are elevated following extraction from the soil for excessive marine growth, damage, and status of the cathodic protection anodes.
- (5) Begin elevating the hull about one foot to check that the elevating system is operating properly. The legs should be lowered sequentially to allow the generators to recover from the start-up loads. While jacking, maintain the hull level within 0.3° to prevent binding of the legs within the guides.

- (6) Contact each leg observer and verify the proper operation of the elevating system.
- (7) Begin lowering the hull to about five feet above the wave crests.
- (8) Hook up the tugs to the unit.
- (9) Lower the unit into the water stopping at about five feet draft and again at ten feet draft. When stopped, check for leaks in all the pre load tanks, inner bottom tanks and voids, mud pits, and machinery deck spaces. If flooding is found, elevate the unit out of the water and correct the malfunction.
- (10) Change to internal drill water cooling, raise the raw water tower to its afloat position, secure it, and re-connect the cooling to the raw water system.
- (11) Instruct the tow vessels to hold the unit from drifting while the spud cans are being extracted from the soil.
- (12) When the legs are free, raise the legs until the reach rod of each spud can drain valve is accessible. Open the drain valves.
- (13) After the drain valves have been opened, raise the legs to their towing position.
- (14) Secure the jacking console and close all elevating motor covers.
- (15) When the hull is refloated and ready for transit, the OIM shall verify that the observed draft, list, and trim agree with the predicted values. Deviations from the predicted values must be accounted for before beginning the tow.

c. Jetting Out

At times the legs cannot be easily extracted from the soil. In this condition the hull will be pulled down into the sea by the jacking system. If this occurs perform the following:

(1) The indication of a stuck leg (or possibly two stuck legs) is a significant change in the inclinometer indications. The "bubble" will tend to move away from the stuck leg. In such cases, stop jacking any free leg. Continue jacking the stuck leg until the draft is one foot deeper than the predicted afloat draft.

- (2) When the leg is stuck, avoid placing excessive stresses on the legs and jacking system. At this time the tugs should provide the minimum force to maintain station.
- (3) If the legs remain stuck, use the jetting system. Connect the jetting hoses to the jetting system on the stuck leg.
- (4) Maintain the one-foot excess draft and operate the jetting system until the leg frees itself. The indication of a free leg is a slow return by the rig to a more level attitude without operating the jacking system.
- (5) Maintain equal leg extensions while extracting the three legs from the soil.
- (6) When all legs are free of the bottom continue raising the legs without hesitation until the legs are well clear of the bottom.

6. OPERATIONAL INSTRUCTIONS - AFLOAT

a. Normal Transit Types

(1) Field transit

A field transit is a change in location requiring less than 12 hours voyage to a protected location or to a location where the unit could be elevated. The move may be longer than 12 hours if, during the voyage, the unit is always less than six hours from a safe location or from a location where it can be safely elevated. A field transit should be made only when good weather and calm seas are predicted for the duration of move plus the periods for lowering and elevating the unit. Field transits may be made with full legs erected.

(2) Ocean transit

An ocean transit is a longer move not meeting the requirements for a field transit, or short moves in an area in which the weather cannot be accurately predicted.

(3) Floating Conditions

There are two primary floating conditions to consider.

Normal Transit condition means that the wind speeds are 70 knots or less. The jack-up may be in a field or ocean configuration. In either case, the TOC must be in the proper position (1.2 feet for field transit and 12.38 feet for ocean transit). The motions of the jackup during a normal transit are limited by leg strength as shown on the upper curve (B) of the Design Limits of Legs (Afloat) Graph. See page 5-7 for the graph on the motions permitted for the Coastal Driller while afloat.

Severe Storm condition is defined as a weather condition in which the expected winds exceed 70 knots. In this condition the legs must be lowered so that the spud can tips are 60.50 feet below the hull in order to meet the stability and leg strength requirements. (See table below for topside indications of leg positions.) Allowable unit motions are defined by curve A of the Design Limits of Legs (Afloat) Graph.

WARNING

When preparing for afloat operations, check that the unit can meet the severe storm allowable KG by only lowering the legs so that TOC is at 60.50 feet below the hull.

b. Limits of Service Afloat

- (1) The load line draft is 10.88' (10' 10.5") feet. Load line marks are found on both sides of the hull approximately 119.5 feet AF0.
- (2) At drafts equal to or less than the load line draft, the Allowable KG must be taken from the appropriate Maximum Allowable KG curve. This value must not be exceeded.
- (3) While operating in this condition, the appropriate leg horizontal must be aligned in the center of the upper guide structure of the gear units.

TIP OF CAN (FT. BELOW B.L.)		LEG POSITION DESCRIPTION	
a.	1.20	Third horizontal centered in upper clamp. (Clamp bar engaged.)	
b.	12.38	Fourth horizontal centered in upper clamp. (Clamp bar engaged.)	
c.	60.50	Eighth horizontal centered in upper clamp. (No clamp bar.)	

c. Operational recommendations - General Afloat

- (1) While underway during a tow, assign trained and experienced personnel to monitor and maintain the seaworthiness of the vessel.
- (2) Maintain current and forecast weather information.
- (3) Verify that the tugs and towing equipment are adequate for the tow.
- (4) Tows should not be made in waters in which floating ice is a hazard, nor should transits be attempted during snow or icing conditions.
- (5) The unit's pitch and roll motions must not exceed the limits shown in the Design Limits of legs (Afloat) Graph (page 5-7). If the limits are approached, reduce the motion by altering tow course or speed. If motions cannot be reduced in this manner, place the unit in the Severe Storm mode.
- (6) Monitor weights, liquids transferred or consumed and equipment relocated during the transit. The load form will require updating as variables are consumed. The OIM must verify that the corrected KG remains below the allowable KG, and that the unit remains at an approximate level attitude.

d. Operational Recommendations - Severe Storm (Afloat)

- (1) Verify that the recommendations for General Afloat (Section C, above) have been performed.
- (2) Recheck the afloat weight distribution calculations using the Severe Storm Maximum Allowable KG Curve.
- (3) Notify the tugs to maneuver to the best towing position for the storm conditions, to minimize the unit's motion.
- (4) Place the unit in the Severe Storm mode. Lowering the legs reduces the wind overturning moments and lowers the KG of the unit, providing greater stability to withstand storm conditions and/or to reduce leg stresses.

e. Changing Modes of Operation Afloat

TIP OF CAN (FEET)		TIME TO LOWER	APPROX TIME
START	END	(MIN.) TOTAL	TOTAL*
1.20	12.38	8	23
1.20	60.50	40	55
12.38	60.50	32	47
	TIP OF (FEE START 1.20 1.20 12.38	TIP OF CAN (FEET) START END 1.20 12.38 1.20 60.50 12.38 60.50	TIP OF CAN (FEET) TIME TO LOWER (MIN.) 1.20 12.38 8 1.20 60.50 40 12.38 60.50 32

(1) Refer to the Mode Transition Table, below, for guidelines regarding the time required to complete the various mode-to-mode operations.

*Includes time to place required generators on-line before lowering legs (approximately 15 minutes).

WARNING

Make any changes in floating mode before the motions become excessive and/or before the wind speed reaches 70 knots.

- (2) When jacking the legs up or down, notify the tugs to hold the unit in position at the directed heading until the jacking is complete, Do not attempt to jack the legs while the unit is being towed. Once the leg position change has been accomplished, resume towing.
- (3) Notify all personnel that jacking is about to begin. Start lowering the legs sequentially, allowing the generators to recover between each start.
- (4) After completion of a mode change, unnecessary generators may be removed from service. Any time involved in reducing the excess generating capacity back to normal is not considered as part of the mode change.
- (5) Reverse the above procedure when returning to the previous mode (times will be the same).

7. EMERGENCY PROCEDURES FOR UNEXPECTED LIST OR TRIM

It is vital to the safety of the unit to maintain watertight integrity, to prevent shifting of loads, and to keep the unit level at a draft which does not exceed 10.88 feet.

When unexpected inclination occurs, the OIM should attempt to determine the cause before taking corrective action. The unexpected inclination often falls into one of three categories, in which inclination:

- · increases rapidly. This situation is critical; immediate action is required.
- increases slowly. This situation is less critical, nevertheless immediate action is required.
- remains constant. Unless the angle is extreme, this case is usually not as severe as the other two cases.

a. Possible causes of unexpected inclination

- (1) Flooding due to external causes. Examples are hull damage or failure of a through-hull fitting.
- (2) Flooding due to internal causes. Examples are piping ruptures, an open valve, or rupture of an internal bulkhead.
- (3) Transfer of liquid. This may be due to inadvertent transfer by personnel or crossflooding through an open valve.
- (4) Shift of load, such as shifting of unsecured cargo in a seaway.
- (5) Miscalculation of loads, such as errors in math or measurement.
- (6) Environmental forces. Heel or trim may be the result of external environmental forces acting on the hull or legs.
- (7) Consumption of onboard liquids, such as fuel oil or drill water.

b. Corrective actions - inclination rapidly increasing

Unless the cause and corrective action are immediately obvious, elevate the unit if at all possible.

Preloading will be required unless the OIM is certain that repairs can be completed within a mild weather window. Elevating the unit will provide time to find the problem and to determine the proper corrective action. Items (1), (2), (3), and possibly (4) may be causes for the rapidly increasing angle of inclination.

Corrective actions should include:

(1) Sound General Alarm and prepare to evacuate non-essential personnel, if deemed necessary by the OIM.

- (2) Check that all watertight doors, valves, and other openings are closed and secured.
- (3) Prepare to pump out adjacent compartments containing liquids.
- (4) Install appropriate devices or fittings to stop or slow flooding. If successful, pump out damaged compartment.
- (5) Consider corrective transfer of onboard liquids.
- (6) If flooding becomes uncontrollable, and the unit is in imminent danger of sinking or capsizing, the OIM shall determine if the unit must be abandoned.

c. Corrective actions - inclination slowly increasing

As with rapidly increasing inclination, elevating the unit may be the best immediate action. However, because the inclination is changing slowly, remaining afloat does not pose as great a threat.

Causes (1), (2), (3), (4), (6), or (7) are the possible causes of slowly increasing angle of inclination.

Corrective actions are the same as those for rapidly increasing inclinations, except that shifting loads should be re-secured. Heel or trim due to environmental forces may require no action.

d. Corrective actions - constant inclination

Constant inclination usually results from a miscalculation in the load form. The cause could be a math error or an error in measurement of one or more loads. One corrective action would be to jack up and recheck the load form.

Other causes of constant inclination could be the inadvertent transfer of onboard liquids, a load shift, environmental forces, or a large quantity of soil on one of the spud cans. One corrective action, would be to assess the situation and, if required, re-level the unit by transfer of liquids.

8. BILGE SYSTEM

This unit is equipped with two independently operated bilge systems, each of which may serve as a backup for the other. The bilge pits are located port and starboard on the machinery deck level, extending below the deck level. (See page 5-28 for a diagram of the layout.) Each bilge pit is monitored by a hydrostatic alarm switch connected to the engine alarm panel with a remote panel located in the OIM's office. In addition, each watertight compartment in the machinery deck has a number of sump valves, at least one of which can be remotely operated from the bilge pit if a flooded compartment cannot be entered to activate the sump valves. A cross-over arrangement is also used to connect the two bilge pits in case one of the pits becomes flooded or inoperable.

A start/stop station for the pumps is located in close proximity to each bilge pit, but the motor starters are located in the MCC. Additional versatility is achieved by having one pump on the emergency switchboard buss. Both suction and discharge lines are six-inch lines. All preload and void tanks are connected to the bilge manifold through independent isolation valves.

Both bilge discharge manifolds provide for direct overboard discharge, or in case of flooding with pollutants, discharge to the skimmer tank for temporary storage. A third discharge is used to activate the raw water header while in the afloat mode.

BILGE SYSTEM OPERATION

General Information

- Keep all valves closed, except when pumping from a tank or compartment.
- The bilge alarm will sound if the bilge pump located in the forward starboard corner of the engine room is left off suction for an extended period.
- 3. Check all bilge sumps periodically to prevent overflows.
- 4. Use the bilge pump located on the same side of the unit as the compartment or sump to be pumped, if possible.

Normal Operation

1. If the compartment or sump is forward of the bilge pits, open the forward valve on the main suction header and close the aft valve. If it is aft of the bilge pump pit, open the aft valve and close the forward valve.

- 2. Close all isolation valves along the main line.
- 3. Close the cross-over valve to the other bilge pit and open the suction valve to the bilge pump.
- 4. If no pollutants are present in the liquid to be pumped, open the overboard discharge valve. If pollutants are present or suspected, open the discharge valve to the skimmer tank.
- 5. Open the sump valve for the compartment to be pumped.
- 6. Turn on the bilge pump.

Operation if One Pump Fails

If one pump fails, and a compartment on that side of the unit needs pumping, open the cross-over valve to the other bilge pit and proceed with normal operation.

Alternative Means of Bilge System Operation

- 1. The salt water eductor may be used as a slower, alternative means of bilge system operation.
- 2. Operation of the salt water eductor system is similar to the bilge system, except that the bilge pumps are not used, and the cross-over valves to the other bilge pit are not closed.
- 3. While elevated, the raw water tower pumps supply the water for the salt water eductor system. While afloat, the fire pumps supply the water.

Bilge System Limitations

If the unit is trimmed or heeled and the bilge pump on the low side of the unit has failed, the pump on the high side may not have enough suction to pump the water out. This condition may require the use of the salt water eductor system on the low side of the bilge pit.

CHAPTER 3 - ELEVATED OPERATIONS

1. PREPARATION FOR ELEVATING

Since the unit is floating when going on location, it is assumed that the OIM has complied with the operational instructions for the afloat mode, and that the unit is in a seaworthy condition when it arrives on location. The new elevation site should be surveyed, the bottom conditions determined, and all obstacles removed before jacking up.

a. Geotechnical Investigations

Geotechnical investigations should be conducted in areas of suspected geological hazards to determine leg penetration, punch-through or bearing failure potential, rig stability during drilling, and possible leg extraction or pullout problems.

In sand or silt bottoms, scouring may occur in which the normal current flow is interrupted by the footings. The result is that soil is carried away.

The prime risk is sudden and unexpected penetration through thin sand layers overlying soft clays. A sudden pentration of one leg may lead to excessive inclination and damage to legs and jacking mechanisms.

During extreme storm conditions, the foundation expriences both horizontal and vertical loading which may exceed the bearing capacity of the soil.

In soft to firm clays, spud cans may penetrate to depths which require pullout forces greater than that which can be supplied by the buoyancy of the hull, which may necessitate extensive jetting.

b. Safe Motion for Going-On Location

In the transit condition the legs are nearly fully elevated and supported as long cantilevers in the hull. Any rolling or pitching motion in combination with wind induces large bending moments in the legs and large reaction forces in jackhouses and supporting hull structures.

Before the legs can be jacked down, the weather forecast and sea state must be checked to ensure that rig motions throughout the elevating period will be within acceptable limits. The Safe Motion for Going-On Location curve, Page 5-8 shows the limits of pitch and roll motions for various water depths.

Periodically, during the elevating operation, check the unit's motion against the curve.

Elevating shall be performed when the seas are less than five feet. This limitation should prevent extreme heave motions, and should also prevent environmental forces from overloading the unit during preloading.

c. Checklist for elevating

- (1) Place generators on line.
- (2) Verify that the motor brake release mechanisms and the gear trains are in operable condition.
- (3) Open all elevating motor covers to reduce the heat load on the motors.
- (4) Advise all personnel that jacking is about to begin. Instruct the leg observers to lubricate the leg racks, guides, and gear mechanisms, and to observe the legs for damage that may have occurred during the tow.
- (5) Check each spud can before lowering to ensure that the drain valves are open and that all vents are clear. This will allow the cans to fill completely. The spud cans may collapse if not vented while they are lowered.
- (6) Begin lowering the legs sequentially to allow the generators to recover from the start-up loads. Stop lowering the each leg when the top of the spud can is submerged two to three feet. Allow the cans to fill completely. Then close the drain valve to prevent bottom sediments from entering the spud cans.
- (7) Lower the legs again until they are about 10 to 15 feet above the sea floor.
- (8) Recheck unit motions and location.

WARNING

Damage to the legs and spud cans may result if the unit is allowed to drift as the spud cans contact the bottom.

- (9) Change to internal drill water cooling for air compressor, etc.
- (10) Lower the legs to the ocean bottom and elevate the hull to the five-foot preload air gap. Maintain the hull level within 0.3° to prevent binding of the legs within the guides.
- (11) Prepare the raw water tower for operation in the elevated position.

2. PRELOADING

Preloading tests the soil to the vertical leg footing reaction that would be imposed by the design storm. This test consolidates the soil under the spud cans and reduces the risk of a large or rapid settling, or even a foundation failure (punchthrough) occurring during drilling or a storm. The environmental forces due to the design storm are simulated by taking onboard an equivalent weight of preload water. This water is then dumped at the end of the preload operation.

The storm leg reaction is the load imposed on each leg footing by the sum of the weight of the unit, the variable, and the environmental forces (wind, waves, and current) on the unit and its legs. This preload leg reaction is calculated by the operator from the full weight of the unit, including lightship, variable, and preload, as determined in the load form.

Preloading must not be carried out in seas greater than 5 feet, in strong or gusting winds, or in strong current conditions. Preloading in such conditions would result in uneven leg reactions, possibly leading to a punch-through during the preload operation, or during a severe storm.

Because excessive air gap could lead to greater damage and/or injury if a punchthrough occurs during the preload operation, the hull bottom should be less than five feet above the wave crests during preloading.

WARNING

Under no circumstances will the unit be preloaded with an air gap greater than five feet.

a. Preloading Procedures

- (1) Determine the preload distribution necessary to provide static loading of *at least* 7,099 kips on each of the three legs. In fact, it is better to go over rather than under, as 200 kips extra preload is allowed, with up to 100 kips extra on a single leg.
- (2) The capacity of the preload tanks is greater than the required preload. This excess capacity provides the flexibility so that the total elevated load, including preload, can be equally balanced on the three legs.
- (3) Add the preload while maintaining equal leg loading and attitude within 0.3° of level. If the total weight is less than 14,400 kips, the low corner of the hull may be raised. At greater weights, the attitude may be controlled by lowering the high corners of the hull.

- (4) As settling occurs, the five-foot air gap decreases. Before the hull enters the water, dump the preload to attain a total weight less than 14,400 kips. The jacking motors may be used to elevate the platform if the total weight is less than 14,400 kips.
- (5) When the five-foot air gap has been re-established, pump the preload water back onboard. Soft bottoms permit greater settling, and may require that this process be repeated several times.
- (6) Maintain final preload for three hours after all settling has taken place and the unit is stabilized.
- (7) Discharge all preload so that the preload remains equally distributed on the three legs during the operation.
- (8) Close all preload dump valves after the preload has been discharged.

WARNING

As much as 500 kips of water may remain in the preload tanks after the dump valves have been opened. This water must be removed or accounted for as part of the variable load.

b. Elevating Procedures

- (1) Elevate the hull to the applicable air gap while maintaining the hull level within 0.3°.
- (2) Place a set of horizontal leg braces as near as possible to the center of the lower hull guides.
- (3) When the hull is elevated, secure the jacking console, and activate the OUT-OF-LEVEL ALARM, and close all elevating motor covers.

3. ELEVATED OPERATIONS

This section provides guidelines for elevated operations under normal conditions and during a severe storm:

Normal Drilling

In this condition, the unit is on location to perform drilling or related operations, and can operate within the environmental limits of the Allowable Wind and Wave Charts (pages 5-9 through 5-20). The charts give the various combinations of wind, waves, and current in which elevated opera-
tions are permitted for a given leg reaction and water depth. If the predicted weather conditions exceed these combinations, the unit must be placed in the elevated Severe Storm mode.

Severe Storm

In this condition, the unit is prepared to withstand environmental forces exceeding the normal drilling criteria. This condition requires that drilling operations be suspended, and that leg reactions be made equal. When a severe storm threatens, the procedures listed in Operational Instructions -Severe Storm (page 3-8) must be implemented.

The Limits of Service - Elevated, page 5-21, shows the maximum wind, wave, and current the unit can withstand for the stated water depths and air gaps.

4. LEG REACTION

The total leg reaction is the load on each leg footing due to unit weight, variable loads, drilling loads, and environmental forces. The environmental forces (wind, waves, and current) on the unit and its legs vary considerably. They are accounted for in the unit's design as a range of environmental limits for a given leg reaction. This leg reaction is calculated in the load form from the lightweight, fixed loads, variables, and drilling loads.

If either the environmental conditions or maximum allowable leg reactions are exceeded, the Coastal Driller and its crew may be placed at risk. The OIM shall monitor the weather and leg reactions daily, and more often if necessary, to ensure that neither the environmental forces nor leg reactions exceed the limits shown in the Allowable Wind and Wave During Drilling charts and Limits of Service Elevated for the elevated storm condition.

The Allowable Wind and Wave During Drilling charts are shown on pages 5-9 through 5-20. These charts give the various combinations of wind, wave, and current in which drilling is permitted. Notice that the highest wind velocity shown on the charts is 70 knots. Should the predicted weather exceed these combinations, the rig must be taken out of the drilling mode and placed in the elevated storm mode.

The Limits of Service - Elevated are displayed in a table on page 5-21. These limits show the maximum wind and wave the Coastal Driller can withstand. If higher wind and waves are expected, the OIM must make suitable arrangements for the evacuation of the rig.

5. OPERATIONAL INSTRUCTIONS - NORMAL DRILLING

a. General Elevated Instructions

Before beginning any elevated operations, the OIM shall ensure that the following operations have been completed satisfactorily:

- (1) Preloading operations completed and load form calculations checked.
- (2) Preload water has been removed, and that the unit is level within 0.3° at the applicable severe storm air gap as stated in the Limits of Service - Elevated, page 5-21.
- (3) Verify that the elevating system is ready for emergency use.
- (4) Make sure the Out-of-Level Alarm is functional at all times.
- (5) Monitor current and predicted weather to evaluate the operating criteria, and to help predict conditions that may require placing the unit in the elevated severe storm mode.
- (6) Prepare the unit for drilling operations by placing the drilling assembly in the desired drilling position. Lubricate all skid rails, and skid the assembly using the longitudinal and transverse skidding motors.

IMPORTANT

Be sure that the drilling structure clamps are released for the skidding operations. After the drill floor is positioned, re-secure the clamps.

(7) Complete load form. Refer to Chapter 4 for guidance on completing the load form.

Record the drilling loads (hook, rotary, setback, and conductor tension), their centers of gravity, and the longitudinal position of the cantilever beams, and drill floor transverse position. Check that each of the drilling loads do not exceed the limits shown in the Cantilever Beam Load Charts, page 5-22.

- (8) Calculate the leg reactions for each leg.
- (9) Determine the environmental conditions. A high calculated leg reaction reduces the wind, waves, and current in which the unit can safely operate. Calculations should be carried out as necessary to evaluate the condition of the unit, and to take appropriate corrective action.
- (10) Develop a procedure for removing excess variable loads in the case a severe storm threatens.

b. Allowable Wind and Wave Charts

The Allowable Wind and Wave Charts, pages 5-9 through 5-20, give the combinations of wind, waves, and current in which the unit can operate for a given leg reaction.

WARNING

Failure to keep the unit's leg reactions below those permitted by the allowable wind and wave charts, or the appropriate maximum leg reaction values, overloads the unit, and places the personnel at risk.

The following data must be available to use the charts:

- The largest of the three leg reactions.
- The amount of leg penetration. If the penetration exceeds 25 feet, the water depth value must be increased by the amount of penetration greater than 25'.
- Water depth including astronomical and storm tides.

The procedures for using the charts are as follows:

(1) Select the appropriate chart based on leg length, minimum air gap, water depth, and current for the particular site in question. For water depths and current velocities that fall between charts, use the chart with the next highest values.

- (2) At the Maximum Leg Reaction, read across the chart to determine wave height and wind speed combinations which are permitted.
- (3) Compare the actual or predicted wind and wave values to those shown in the Allowable Wind and Wave Chart. If they are less than the allowable, the unit is in a satisfactory condition. If actual or predicted weather conditions exceed the allowables indicated on the chart, take immediate action to reduce the highest leg reaction. Leg reactions can be lowered by reducing or relocating the variable and/or drilling loads. If leg reactions cannot be reduced sufficiently, prepare the unit for the Severe Storm mode.

6. OPERATIONAL INSTRUCTIONS - SEVERE STORM (ELEVATED)

- a. Suspend drilling operations well in advance of the anticipated storm.
- b. After suspending drilling operations, the time required to place the unit in Severe Storm mode should not exceed six hours. Complete the following procedures:
 - (1) Check that the hull is level within 0.3°. Confirm that the unit is at the correct air gap. For stonger support, locate a set of horizontal leg braces as near as possible to the center of each lower hull guide, as footing penetrations permit.
 - (2) Reduce variable loads to no more than the maximum permitted during elevated severe storm conditions.
 - (3) Remove all setback from the derrick and account for its weight as a variable load.
 - (4) Secure the well and drill floor equipment.
 - (5) Skid the cantilever beams and/or subbase to the full forward storm position and secure.
 - (6) Change over to drill water cooling and raise the raw water tower to the full up position and secure.
 - (7) Complete an elevated load form to check the previously prepared storm form. Recompute the new LCG and TCG. If necessary, adjust the loads on the unit so that LCG = 119.44 AF0 and TCG is zero. This insures that the leg reactions are balanced and do not exceed the Maximum Allowable Elevated Storm Leg Reaction.

- (8) Check that the unit is storm-ready by:
 - · Closing all watertight doors, openings, and valves.
 - Securing the tubulars in the pipe rack.
 - Lashing all derrick lines.
 - Securing all movable objects.
- (9) Check horn, navigation lights, and other safety equipment.
- (10) Take suitable action to provide for the safety of all personnel.
- (11) Check that the elevating systems are ready for emergency operations.
- (12) Check that the Out-of-Level Alarm is functional.

7. LIMITS OF SERVICE - ELEVATED

The limits shown in the Limits of Service - Elevated (page 5-21) are based on the following:

- a. Soil penetration is assumed to be 25 feet. If the penetration exceeds 25 feet, the water depth value must be increased by the amount of additional penetration. For example, if the penetration is 50 feet and the actual water depth is 175 feet, the water depth value is adjusted to 200 feet.
- b. When preloaded properly, the reaction on each of the three legs is 7,099 kips. (Total unit weight is 21,297 kips.)
- c. During a severe storm, the sum of the solid and liquid variables must not exceed 2,381 kips.
- d. The water depth shown in the Limits of Service includes all tides, both astronomical and storm.
- e. The air gap shown in the Design Criteria is measured between the charted water depth including allowances for astronomical and storm tides and the bottom of the hull. (Because of the waves, the distance between the wave crests and the hull bottom will be less.) These distances are illustrated in the figure on the following page.

Illustration of Air Gap Computation



WARNING

Use of air gaps other than stated in this manual could result in overloading the unit. Lower air gaps could position the hull in the storm wave zone. Larger air gaps could increase the over-turning moments.

8. EMERGENCY INFORMATION

- a. It is vital to the safety of the unit and its personnel that the hull be kept above the wave action.
- b. In other than afloat conditions, the hull must be maintained level. If inclination exceeds 0.3°, level the unit by:
 - (1) Lowering the high corner(s), but keep the hull above all wave action.

WARNING

Raise the low corner(s) of the unit only if lowering the high corner(s) places the unit in the wave action.

- (2) After the hull is level, raise the unit on all three legs to the proper air gap. Inspect the unit for damage.
- (3) Confirm operation of the Out-of-Level Alarm.

9.0 UNIT EVACUATION PROCEDURES

The following procedures apply to evacuating the unit. Because the circumstances which may prevail are so varied, the sequence or appropriateness of each action must be evaluated by the OIM on a case-specific basis.

The guidelines in this section are limited to the actions which are to be performed aboard the unit. For additional guidelines concerning evacuation procedures, refer to the Evacuation Procedure Manual.

- 1. Secure the unit as in preparation for a severe storm.
- If the unit is being evacuated under emergency conditions requiring the use of the unit's lifeboats/liferafts, the abandon unit procedures contained in the unit's station bill are applicable. Evacuation routes are indicated on the posted Fire Control/Life Saving Plan.
- 3. If the unit is being evacuated by helicopter or service boats, perform the following steps:
 - a. Perform an accurate headcount.
 - b. Determine evacuation craft capacities and arrival times. Organize personnel into groups and designate group leaders. Advise all group personnel of their designated leaders. Group leaders shall:
 - 1. Make sure that each member of the group has boarded the evacuation craft.
 - 2. Report that fact (or who is missing) to the OIM.
 - 3. Board the evacuation craft last.

- c. Evacuate non-essential personnel such as galley hands, off tour personnel (unless needed for specific tasks), third party personnel, visitors, etc. If the approach of a severe storm is the reason for evacuating the unit, all non-essential personnel should be off the unit 48 hours in advance of the storm's arrival, if practical.
- d. All personnel should be evacuated before sea, wind, or visibility conditions deteriorate to the point that further evacuation efforts become unduly hazardous. In the case of helicopters, the pilot will usually make the decision when he can no longer fly. However, in the case of transfer to boats, the OIM, in consultation with the boat skipper, will decide when wind, sea conditions, the transfer means, and other pertinent factors add up to an unacceptable risk.
- e. While one of the purposes of emergency evacuation plans is to ensure a timely evacuation, unforeseen circumstances may arise where there may be less risk to the remaining personnel to remain on the unit than to attempt a transfer to an evacuation craft under extremely hazardous conditions. For example, there may be no way for a boat crew to effectively help personnel being transferred to the open deck of a boat in heavy seas. In such cases, remaining on the unit may be less hazardous.
- f. Procedures for evacuating the last person should be discussed in advance. Normally, the OIM would be the group leader for the last group and, therefore, the last man leaving the unit. If the last man off is to evacuate by such means as climbing down a leg or using a slide line, physical ability and willingness should be taken into consideration. If the OIM is not the last man off, he shall oversee personnel accountability activities until he is satisfied that all personnel are accounted for before leaving the unit.

CHAPTER 4 - STABILITY CALCULATIONS

This Chapter describes the manual calculations necessary to assess the afloat and elevated stability of the Coastal Driller. Emphasis is on the use of the Load Form to assist in the calculations. The Chapter is organized as follows:

- Section 1 describes how the Load Form is organized, and how it is completed. The calculations necessary for completing each of the topics on the Load Form are specifically addressed.
- Section 2 describes how afloat stability is assessed.
- Section 3 explains the method for calculating leg reactions.
- Section 4 describes a method for calculating the preload distribution.
- Section 5 provides sample load forms in which the methods and procedures described above are used.

1. LOAD FORM ORGANIZATION

The purpose of the load form is to formalize the collection of inventory data so that a stability assessment can be made. The load form is the basis from which assessments of afloat stability and leg reactions are made. Beginning with lightweight and center of gravity, an accurate accounting is made for every weight added, discharged, or shifted in order to determine the composite weight and the location of the unit's center of gravity. In the afloat condition, weight and all three components of the center of gravity (LCG, TCG, and VCG) are used to predict the unit's stability, draft, list, and trim. In the elevated mode, total weight, LCG, and TCG are used to calculate the leg reactions.

The load form is organized to use moment theory to find the coordinates of the center of gravity for a group of loads by solving in tabular form, the following general equation:

$$CG = \frac{\sum (w \times cg)}{\sum (w)}$$

In this expression, CG refers to the coordinate of the center of gravity location for a group of weights, "w" is the weight of a component within the group, and "cg" is a coordinate of the center of gravity of that weight. " Σ " means "the sum of".

The Coastal Driller load form consists of three sheets, each of which in practice may consist of one or more pages. The three sheets are:

a. • Sheet 1 - Summary

Sheet 1 contains the Load Summary in the upper half and the Stability and Leg Reaction Summary in the lower half.

The upper portion of the Load Summary tabulates the entries for determination of lightweight and its centers of gravity considering the variable position of the cantilever, drill floor, and legs.

The variable loads consisting of the changes to basic hull, cantilever beam assembly, and drill floor, Solid Variables (Sheet 2), and Liquid Variables (upper portion of Sheet 3) are then entered in the table.

The preload, if present, is the next entry in the load form.

The hook load, is then added in the load summary. Because the position of the drill floor influences the stresses in the cantilever beam, the limiting values of drilling loads (combined hook, rotary, conductor tension, and setback) are given in the cantilever beam load chart. See page 5-22 for the cantilever beam chart.

Each of the five moment columns are added to obtain the total LM, TM, VM, FSML, and FSMT. Dividing LM, TM, and VM by displacement yields the components of the center of gravity for the loaded jackup.

$$LCG = \frac{\sum LM}{\sum W}$$
$$TCG = \frac{\sum TM}{\sum W}$$
$$VCG = \frac{\sum VM}{\sum W}$$

The bottom line of the Load Summary (upper table) shows the LCG, TCG, and VCG for the loaded jackup. The VCG is used for afloat stability. LCG and TCG are used for both afloat and elevated calculations. When afloat, LCG and TCG are used for list and trim calculations. When elevated, LCG and TCG are used in the calculations for leg reactions.

Stability assessment for the afloat and elevated modes is discussed in Sections 2 and 3 of this chapter.

Sheet 2 - Solid Variable Loads

Sheet 2 is the result of a careful deck survey for the solid variables, such as tubulars, cement, and barite . It serves as "input" data for the solid variable figures in Sheet 1. Note that some of the solid variables are located on the cantilever beam (lower portion of Sheet 2), and therefore, change longitudinal position as the cantilever is skidded fore and aft. Weights and center of gravity locations of all solid variables are entered in Sheet 2.

- For an afloat analysis, enter all three coordinates of the center of gravity (VCG, LCG, and TCG).
- For an elevated analysis, enter only LCG and TCG.

Multiply each weight by its components of the center of gravity coordinates to obtain longitudinal, transverse, and (if afloat) vertical moments.

Sum the weights and moments, and enter the values for solid variables in the summary table on Sheet 1.

c.

b.

Sheet 3 - Liquid Variable Loads & Preload

Data for Sheet 3 is also the result of a careful deck survey for the liquids. The upper portion is for liquid variables; the lower is for preload.

Weights, centers of gravity, and free surface moments of all liquids are entered in Sheet 3 according to the following guidance:

(1) Afloat

Enter the three coordinates of the center of gravity (VCG, LCG, and TCG). In addition, for each slack tank, enter the free surface moments (FSML and FSMT) shown in the appropriate tank tables.

(2) Elevated

Enter only LCG and TCG. Because the legs are on the bottom, vertical moments and free surface moments are not necessary.

In each case, afloat or elevated, multiply the weight by its center of gravity component to obtain LM, TM, and if afloat, VM. The weights and moments, including free surface moments, for the liquid loads are then summed and entered on the Load Summary, Sheet 1.

4-3

2. AFLOAT STABILITY

a. Hydrostatic Data

For hydrostatic data, use the Table of Hydrostatic Properties, pages 5-4 and 5-5. Interpolation may be required.

(1) Draft

Extract the draft for the calculated displacement from the Hydrostatic Properties Table, pages 5-4 and 5-5.

Compare the calculated draft with the values at the draft marks. The observed draft should not exceed 10.88 feet (10' 10.5"). The calculated displacement must not exceed the maximum load line displacement (14,158.31 kips).

If either the maximum displacement is exceeded or the load line (Plimsoll Mark) is submerged, weight must be removed from the unit.

WARNING

The draft must not exceed 10.88 feet.

(2) LCB

The longitudinal location of the center of buoyancy (LCB) is used in the trim equations. Extract the data from the Table of Hydrostatic Properties, pages 5-4 and 5-5, for the weight in the Loaded Displacement line.

(3) KML and KMT

KML and KMT are used in calculations involving initial stability. They are obtained from the Hydrostatic Properties Table, pages 5-4 and 5-5, for the calculated loaded displacement. Interpolation may be necessary.

b. Stability Data

(1) Maximum Allowable KG

Stability is evaluated by comparing the higher of the two corrected KGs with the maximum allowable KG. The stability limits for the Normal Transit and Severe Storm modes are shown in the maximum Allowable KG Curves, page 5-6. These two curves provide the maximum allowed KG for a specific draft depending on the wind speed (70 or 100 knots). If the corrected KG is less than the maximum allowed, stability is acceptable.

(2) Free Surface Corrections

The free surface corrections (FSCL and FSCT) are obtained by dividing the sum of the free surface moments in both the transverse and longitudinal modes (FSMT and FSML) by displacement. Because the tanks are wall-sided with rectangular cross-section, the free surface moments are constant over the range of soundings, unless the tanks are pressed or empty. FSML and FSMT are tabulated in the tank tables.

$$\mathsf{FSCL} = \frac{\sum \mathsf{FSML}}{\Delta}$$

$$\mathsf{FSCT} = \frac{\Sigma \, \mathsf{FSMT}}{\Delta}$$

(3) Corrected Height of the Center of Gravity

The uncorrected KG is listed in the bottom line of the Load Summary. The free surface correction from above is then added to KG to obtain KGL and KGT.

> KGL = KG + FSCLKGT = KG + FSCT

(4) Metacentric Height

GMT and GML is used to evaluate initial stability, and to compute the predicted value of trim and list. It is computed by subtracting the corrected KGs from the appropriate KMs.

$$GMT = KMT - KGT$$

 $GML = KML - KGL$
 $4-5$

c. Trim and List

Trim

Inclination in the longitudinal mode is called trim. It may be measured in feet as the difference in drafts at the forward and aft draft marks, or in degrees as an angle of inclination in the longitudinal sense. The equations for calculating trim in either feet or degrees are shown below. Although the accuracy of the formula for finding trim in *degrees* diminishes as angles of inclination increase above 15°, this method is sufficient at small angles. Trim by the stern (stern down or bow up) is considered positive. Thus, trim by the head (bow down) is considered negative.

 $Trim = \frac{(LCG - LCB) L}{GML}$ (Feet)

$$Trim = \frac{(LCG - LCB) 57.3}{GML}$$
 (Degrees)

List

Inclination in the transverse mode, if caused by off-center loading, is called list. If caused by an external force, it is called heel. Either may be expressed in feet or degrees. As feet, it is the difference between drafts at the extreme starboard and port draft marks. In the formula below, B is the extreme transverse distance between draft marks. The second formula, below, gives the angle of transverse inclination. Although the accuracy of the formula for finding list in *degrees* diminishes as angles of inclination increase above 15°, this method is sufficient at small angles.

For the Coastal Driller, inclinations which result in the starboard side being down (port side up) are considered positive.

List = $\frac{TCG \times B}{GMT}$ (Feet) List = $\frac{TCG \times 57.3}{(Degrees)}$

d. Drafts

Drafts at each of the four draft marks are calculated by proportioning the trim and list values (in feet) as draft corrections at the draft marks. The equations for the draft at each of the four draft marks are:

DraftsFDM = DraftcF - 0.666 x Trim + 0.214 x List DraftPFDM = DraftcF - 0.666 x Trim - 0.214 x List

GMT

 $DraftsADM = DraftcF + 0.334 \times Trim + 0.500 \times List$ $DraftPADM = DraftcF + 0.334 \times Trim - 0.500 \times List$

The forward draft marks are on each side of the hull, 38.12 feet AF0, and 37.69 feet port and starboard of the centerline. The aft draft marks are also on each side of the hull, 160.17 feet AF0, and 88.0 feet port and starboard of the centerline. From the hydrostatic tables, LCF is 119.44 feet AF0, and TCF is zero.

3. LEG REACTION CALCULATION

Once the Total Calculated Weight and its LCG and TCG are determined, the leg reactions can be easily calculated using the formulas below. For convenience, the Leg Reaction Calculation Form, shown on page 5-24, may be used to organize the computations.

Taking moments about an axis connecting the aft legs results in the following expression for the bow leg reaction:

Bow Leg Reaction = $\frac{W(160 - LCG)}{121.67}$

The calculation for the aft leg reactions is based on taking moments about an axis parallel to the longitudinal axis through one of the aft legs as shown in the sketch below:



Taking moments about the port leg results in the following equation for the reaction in the starboard leg:

Starboard Leg Reaction =
$$\frac{W(60 + TCG) - (Bow \times 60)}{120}$$

When moments are taken about the starboard leg, the following expression for the port leg reaction is obtained:

Port Leg Reaction =
$$\frac{W (60 - TCG) - (Bow \times 60)}{120}$$

EXAMPLE: Find the leg reactions for the elevated Coastal Driller when the following conditions exist:

W LCG	= =	15,000 kips 125.0 feet AFO
TCG	=	- I.0 feet (port of centerline)
Bow Leg Reaction	= <u>W (1</u>	<u>60 – LCG)</u> 121.67
	= <u>15.0</u>	<u>00 (160 – 125)</u> 121.67
	= 4,31	5 kips
Starboard Leg Reaction	= <u>W (6</u>	<u>120 + TCG) – (Bow x 60)</u> 120
	= <u>15.0</u>	00 [60 + (– 1)] – (Bow x 60) 120
	= 5,21	7 kips
Port Leg Reaction	= <u>W (6</u>	<u>60 – TCG) – (Bow x 60)</u> 120
	= <u>15,0</u>	<u>00 [60 – (– 1)] – (Bow x 60)</u> 120
	= 5,46	8 kips

4. PRELOAD DISTRIBUTION CALCULATION

The following method illustrates a method to determine the preload distribution so that the leg reactions are equal at 7,099 kips.

With twelve preload tanks and many combinations of initial list and trim, the problem can be complex. To reduce the problem to a level that can be handled easily, several simplifying conditions are established.

First, the jackup should have zero list. This condition is not difficult to meet, and in all likelihood exists, in any event, when going on location. Had there been some list in transit, fuel oil or drill water would have been transferred to level the vessel. The advantage to using fuel oil or drill water to level the vessel transversely is that the preload water can be loaded symmetrically.

Second, the problem of distributing the preload can be simplified further by using the concept of core tanks. The core tanks are defined as tanks 8, 9, 15, 16, 21A, 22A, 21B, and 22B. They are always filled to 20.0 feet sounding during preloading. When full, the sea water in the core tanks weighs 4,991.5 kips, and provides longitudinal moments of 616,946 ft-kips. Because these tanks are not exactly symmetrical, some transverse moments (-1,946 ft-kips) will be created. These unbalanced moments will be reduced later.

Third, the problems can be simplified even more by treating the two forward tanks (tanks 2 and 3) and the two aft tanks (tanks 28 and 29) as single tanks located on the centerline. The LCG of the forward pair is 28.87 ft AF0, and the LCG of the aft pair is assumed is 188.82 ft AF0.

Since the core tanks provide a fixed amount of weight and LM, the problem of distributing the preload is reduced to loading sufficient weight in the "combined" tanks so that the total reaction of the three legs is 21,297 kips, and the total longitudinal moments are 2,543,714 ft-kips. When these conditions are met, each of the three leg reactions will be 7,099 kips.

The specific steps to calculate the ballast distribution are:

- a. Using a blank preload calculation sheet similar to that shown on page 5-25, enter the floating displacement and longitudinal moments in the appropriate blanks.
- b. Subtract the sum of the weights in the first two lines from 21,297 kips. Enter the result on the third line under Weight. This value is the weight needed to place the total unit weight in the required preload condition.
- c. Subtract the sum of the LM in the first two lines from 2,543,714 ft-kips. Enter the result on the third line under LM. These are the LM needed to place the total unit LM at 119.44 feet AF0.
- d. The needed weights and moments must be supplied by the proper combination of preload in the two "combined" fore and aft tanks.

e. Using the equation below, the weight in the forward combination can be calculated.

 $Wt Fwd = \frac{(188.82 \times Wt Needed - LM Needed)}{159.95}$

f. The weight calculated for the forward combination is then evenly split between tanks 2 and 3. The sounding level is easily calculated by dividing by the weight per foot of preload in that tank.

Tank 2	Weight	= 0.5 x Wt Fwd
	Sounding	= <u>Weight</u> 49.596
Tank 3	Weight	= 0.5 x Wt Fwd
	Sounding	$= \frac{\text{Weight}}{50.356}$

g. The weight needed in the aft combination is obtained by subtracting the weight in the forward combination from the total needed.

Wt Aft = Wt Needed - Wt Fwd

h. Because the preload tanks are not exactly symmetrical, a small unbalanced transverse moment to port is created which can be eliminated by transferring 29 kips from tank 29 to tank 28. The weight and sounding levels in the two aft tanks now become:

Tank 28	Weight	= 0.5 x Wt Aft + 29
	Sounding	$= \frac{\text{Weight}}{42.554}$
Tank 29	Weight	= 0.5 x Wt Aft - 29
	Sounding	$= \frac{\text{Weight}}{43.314}$

7. SAMPLE LOAD FORMS

The following sample load forms are provided in the following pages:

a. #1 (Rig Move)

Displacement 14,158.3 kips Draft 10.88 ft Variable Load 2,381.1 kips Cantilever 28.33 ft fwd of transom Level Attitude

b. #2 (Preload)

Total Weight21,296.7 kipsVariable Loads2,381.0 kipsPreload7,138.4 kipsCantilever28.33 ft fwd of transomWater Depth250.0 ft

c. #3 (Drilling)

Total Weight15,435.9 kipsVariable Loads3,381.0 kipsCantilever40.0 ft aft of transom, 8.0 ft to portWater Depth250.0 ft

d. #4 (Elevated Severe Storm)

Total Weight	15,158.3 kips
Variable Loads	2,381.0 kips
Cantilever	28.33 ft fwd of transom
Water Depth	250.0 ft

COASTAL DRILLER Load Calculation Form



Rotary fwd of transom = 28.33 feet Rotary relative to C/L = 0.00 feet on centerline TOC below baseline = 1.20 feet

SHEET 1 - SUMMARY SHEET

SUMMARY - LOAD TABLE

Item	Weight kips	LCG feet	LM ft-kips	TCG feet	TM ft-kips	VCG feet	VM ft-kips	FSML ft-kips	FSMT ft-kips
Hull - Basic & Fixed Loads	7068.90		787118		15339		138126		
Cantilever Beam Loading	870.00		136755		-1523		28580		
Drill Floor & Equipment	580.00	1.1.1.1.1	107138	_	220		40733		
Legs 360.33 ft	3258.30		389173		0	135.04	440002		
LIGHTWEIGHT	11777.20		1420184		14037		647441	1	
Changes to basic hull	77.30		10896		1757		1675		
Changes to cant. beam assembly	10.00	160.00	1600		-190		280		
Changes to drill floor	11.20	196.89	2211	-17.75	-199		400		
SOLID VARIABLES	1123.40		151524		-19851		33433		
LIQUID VARIABLES	1159.20		104595		4443		2195	31677	25098
PRELOAD	0.00		0		0		0	0	0
HOOK LOAD	0.00	0.00	0	0.00	0		0		l
LOADED DISPLACEMENT	14158.30		1691010		-4		685424	31677	25098
CG Location		119.44		0.00		48.41			

	STA	BILITY & LEG	REACTIO	ON SUMMARY
	AFLOAT S	LEG REACTIONS		
HYDRO DATA	TRIM	LIST		
Draft (feet) LCB (feet)	10.88	Trim 0 Trim 0	.00 deg	BOW LEG Reaction NA ki
KML (feet) KMT (feet)	249.09 134.40	List 0 List 0	.00 deg	PORT LEG Reaction NA kij
				Water depth NA fe
STAB DATA		DRA	FTS	
KGmax 70 Kts (feet)	65.00	Stbd-Fwd	10.88 feet	TOTAL WEIGHT 14158 kir
KGmax 100 Kts (feet) FSCL (feet)	39.00	Port-Fwd Stbd-Aft	10.88 feet 10.88 feet	et VARIABLE LOADS 2381 kip
FSCT (feet) KGL (feet)	1.77 50.65	Port-Aft	10.88 feet	VAR LOADS MARGIN 0 kip
KGT (feet) GML (feet)	50.18 198.44			
GMT (feet)	84.21			

FORM #1 RIG MOVE

SHEET 2 - SOLID VARIABLE LOADS

Ullage	Weight	LCG	LM	TCG	TM	VCG	VM	
feet	kips	feet	ft-kips	feet	ft-kips	feet	ft-kips	
0.00	188.10	128.00	24077	-67.00	-12603	30.50	5737	
5.78	133.70	128,00	17119	-53.00	-7088	28.00	3745	
6.00	68.20	128.00	8727	53.00	3614	27.50	1875	
17.35	12.90	128.00	1652	67.00	865	24.00	310	
	6.00	77.00	462	0.00	0	7.50	45	
	5.00	156.00	780	0.00	0	7.50	38	
	5.00	156.00	780	30.00	150	7.50	38	
	0.00	131.00	0	35.00	0	8.00	0	
	10.00	190.00	1900	39.00	390	41.00	410	
	10.00	67.60	676	-32.00	-320	7.00	70	
	106.00	138.00	14628	-40.00	-4240	8.50	901	
	18.00	78.00	1404	0.00	0	35.00	630	
	0.00	126.25	0	0.00	0	0.00	0	
	8.00	195.00	1560	-50.00	-400	22.00	176	
	8.00	156.00	1248	-52.00	-416	22.00	176	
	8.00	51.00	408	-32.00	-256	23.00	184	
er	6.00	170.00	1020	0.00	0	22.50	135	
	7.00	172.00	1204	-40.00	-280	32.00	224	
	9.40	170.00	1590	-60.00	-561	21.50	201	
	15.00	189.00	2835	58.00	870	24.50	368	
	25.00	138.00	3450	40.00	1000	23.50	588	
	10.00	160.00	1600	52.00	520	20.00	200	
oading	659.30		87119		-18756		16048	
adina								
ading	134.60	128.00	17229	-11.75	-1582	39.00	5249	
	89.20	128.00	11418	15.00	1338	39.00	3479	
	75.50	128.00	9664	-23.75	-1793	37.50	2831	
	64.80	128.00	8294	20.75	1345	37.50	2430	
	15.00	179.00	2685	20.75	311	28.00	420	
	55.00	179.00	9845	-13.00	-715	29.00	1595	
	20.00	179.00	3580	0.00	0	51.00	1020	
	10.00	169.00	1690	0.00	0	36.00	360	
bading	464.10		64405		-1096		17384	
IABLES	1123.40		151524		-19851		33433	
	Ullage feet 0.00 5.78 6.00 17.35 17.35 er oading ading ading IABLES	Ullage feet Weight kips 0.00 188.10 5.78 133.70 6.00 68.20 17.35 12.90 6.00 5.00 5.00 5.00 0.00 10.00 10.00 10.00 10.00 106.00 18.00 0.00 8.00 8.00 8.00 8.00 9.40 15.00 25.00 10.00 0.00 25.00 10.00 25.00 10.00 25.00 10.00 25.00 10.00 25.00 10.00 25.00 10.00 25.00 10.00 25.00 10.00 25.00 20.00 15.00 55.00 20.00 10.00 55.00 20.00 10.00 0.00 10.00 0.00 20.00 10.00 20.00 10.00	Ullage feet Weight kips LCG feet 0.00 188.10 128.00 5.78 133.70 128.00 6.00 68.20 128.00 17.35 12.90 128.00 5.00 156.00 5.00 156.00 0.00 131.00 10.00 190.00 10.00 190.00 10.00 190.00 10.00 18.00 106.00 138.00 18.00 78.00 0.00 126.25 8.00 195.00 8.00 156.00 25.00 17.00 7.00 172.00 9.40 170.00 15.00 189.00 25.00 138.00 10.00 160.00 0 25.00 134.60 128.00 75.50 128.00 75.50 128.00 15.00 179.00 55.00 179.00	Ullage feet Weight kips LCG feet LM ft-kips 0.00 188.10 128.00 24077 5.78 133.70 128.00 17119 6.00 68.20 128.00 8727 17.35 12.90 128.00 1652 6.00 77.00 462 5.00 156.00 780 5.00 156.00 780 0.00 131.00 0 10.00 190.00 1900 10.00 67.60 676 106.00 138.00 14628 18.00 78.00 1404 0.00 126.25 0 8.00 156.00 1248 8.00 150.00 1248 9.40 170.00 1020 7.00 172.00 1204 9.40 170.00 1590 15.00 189.00 2835 25.00 138.00 3450 10.00 160.00 1600	Ullage feet Weight kips LCG feet LM ft-klps TCG feet 0.00 188.10 128.00 24077 -67.00 5.78 133.70 128.00 17119 -53.00 6.00 68.20 128.00 8727 53.00 17.35 12.90 128.00 1652 67.00 5.00 156.00 780 0.00 5.00 156.00 780 30.00 0.00 131.00 0 35.00 10.00 190.00 1900 39.00 10.00 67.60 676 -32.00 106.00 138.00 14628 -40.00 18.00 78.00 1404 0.00 0.00 126.25 0 0.00 8.00 51.00 408 -32.00 er 6.00 170.00 1204 -40.00 9.40 170.00 1204 -40.00 9.40 170.00 1590 -60.00	Ullage feet Weight kips LCG feet LM feet TCG feet TM feet 0.00 188.10 128.00 24077 -67.00 -12603 5.78 133.70 128.00 17119 -53.00 3614 17.35 12.90 128.00 1652 67.00 865 6.00 77.00 462 0.00 0 5.00 156.00 780 0.00 0 5.00 156.00 780 30.00 150 0.00 131.00 0 35.00 -4240 10.00 67.60 676 -32.00 -320 106.00 138.00 14628 -40.00 -4240 18.00 78.00 1404 0.00 0 8.00 195.00 1560 -50.00 406 8.00 151.00 408 -32.00 -256 er 6.00 170.00 1020 0.00 0 9.40 170.00 159	Uilage feet Weight kips LCG feet LM feet TCG feet TM ft-kips VCG feet 0.00 188.10 128.00 24077 -67.00 -12603 30.50 5.78 133.70 128.00 17119 -53.00 -7088 28.00 6.00 68.20 128.00 1652 67.00 865 24.00 5.00 156.00 780 0.00 0 7.50 5.00 156.00 780 30.00 150 7.50 0.00 131.00 0 35.00 0 8.00 10.00 190.00 1900 39.00 39.00 41.00 10.00 67.60 676 -32.00 -320 7.00 106.00 138.00 14628 -40.00 -4240 8.50 18.00 78.00 1404 0.00 0 0.00 8.00 156.00 1248 -52.00 -416 22.00 8.00 170.00 15	Ullage feet Weight kips LCG feet LM ft-kips TCG feet TM ft-kips VCG feet VM ft-kips 0.00 188.10 128.00 24077 -67.00 12603 30.50 5737 5.78 133.70 128.00 8727 53.00 -7088 28.00 3745 6.00 68.20 128.00 1652 67.00 865 24.00 310 6.00 77.00 462 0.00 0 7.50 45 5.00 156.00 780 0.00 0 7.50 38 0.00 131.00 0 35.00 0 8.00 0 10.00 190.00 1900 39.00 390 41.00 410 110.00 67.60 676 -32.00 -320 7.00 70 106.00 128.00 14628 -40.00 -4240 8.50 901 18.00 156.00 1248 -52.00 -416 22.00 176

FORM #1 RIG MOVE

SHEET 3 - LIQUID VARIABLE LOADS

Tank	Sound	Weight	LCG	LM	TCG	TM	VCG	V M ft-kine	FSML	FSMT ft-kins
Potoblo water Tk 4	4.59	157.80	65.36	10311	14.22	2243	2 20	361	1707	1965
Potable water - Tk 5	4.50	157.80	65.36	10311	-14.22	-2243	2.29	361	1707	1965
Fotable water - TK 5	4.50	157.00	00.00	10011	-14.66	-2240	6.60	001	1101	1000
Drill water - #1	4.81	120.50	4.63	558	0.00	0	241	290	181	4580
Drill water - #6	4.81	160.70	78.30	12585	33.51	5386	2.41	387	4464	932
Drill water - #7	1.89	63.20	78.30	4945	-33.51	-2116	0.95	60	4464	932
Drill water - #10	0.61	16.00	85.30	1361	12.08	193	0.31	5	725	1345
Drill water - #11	0.61	16.00	85.30	1361	-12.08	-193	0.31	5	725	1345
Drill water - #17	0.00	0.00	126.16	0	-13.00	0	0.00	0	0	0
Drill water - #18	0.00	0.00	126.91	0	12.17	0	0.00	0	0	0
Drill water - #23	0.94	48.30	156.00	7539	-13.00	-628	0.47	23	4708	2982
Drill water - #24	0.94	48.30	156.00	7539	13.00	628	0.47	23	4708	2982
Drill water - #25	4.08	123.90	154.62	19153	-34.00	-4212	2.04	253	3045	777
Drill water - #26	1.75	53.10	154.62	8215	34.00	1806	0.88	46	3045	777
Diesel oil - #13	2.74	48.90	105.94	5184	-41.41	-2026	1.37	67	404	1034
Diesel oil - #14	5.00	122.00	104.12	12702	39.16	4777	2.50	305	0	0
Diesel oil - #19	0.00	0.00	126.37	0	-42.69	0	0.00	0	0	0
Diesel oil - #20	0.48	16.70	126.71	2110	41.20	686	0.24	4	1774	3474
Dirty oil tank	2.10	6.10	117.16	720	23.00	141	1.00	6	20	8
Mud pit #1 (Stbd)	0.00	0.00	103.66	0	19.50	0	5.00	0	0	0
Mud pit #2 (Stbd)	0.00	0.00	104.67	0	5.85	0	5.00	0	0	0
Mud pit #3 (Port)	0.00	0.00	103.66	0	-6.50	0	5.00	0	0	0
Mud pit #4 (Port)	0.00	0.00	103.66	0	-19.50	0	5.00	0	0	0
Slugging pit	0.00	0.00	97.70	0	10.25	0	5.00	0	0	0
Skimmer tank	0.00	0.00	185.00	0	54.00	0	0.00	0	0	0
Sand traps		0.00	190.00	0	40.00	0	25.00	0	0	0
TOTAL LIQUID VA	RIABLES	1159.20		104595		4443		2195	31677	25098
FRELOAD TANKS	Sound	Waight	100	1 1 14	TCC	TM	VCC	I VA	ECMI	ECMT
Tank	foot	kine	foot	ft-kine	foot	ft-kine	foot	ft-kinc	ft-kine	ft_kinc
Preload Tank # 2	0.00	0.00	28.89	0	23.28	0	0.00	0	0	0
Preload Tank #3	0.00	0.00	28.85	0	-23.35	0	0.00	0	0	0
Preload Tank # 8	0.00	0.00	69.17	0	44.46	0	0.00	0	0	0
Preload Tank # 9	0.00	0.00	68.17	0	-43.71	0	0.00	0	0	0
Preload Tank #15	0.00	0.00	103.66	0	-59.26	0	0.00	0	0	0
Preload Tank #16	0.00	0.00	103.66	0	59.26	0	0.00	0	0	0
Preload Tank #21A	0.00	0.00	141 75	0	-74.95	0	0.00	0	0	0
Preload Tank #22A	0.00	0.00	141.65	0	74 98	0	0.00	0	0	0
Preload Tank #21B	0.00	0.00	184.06	0	-65.02	0	0.00	0	0	0
Preload Tank #22B	0.00	0.00	184.05	0	65.77	0	0.00	0	0	0
Preload Tank #28	0.00	0.00	188.86	0	36.10	0	0.00	0	0	0
Preload Tank #29	0.00	0.00	188.79	0	-36.28	0	0.00	0	0	0
TOTAL PRELOAD		0.00		0		0		0	0	0

COASTAL DRILLER Load Calculation Form



Rotary fwd of transom = 28.33 feet Rotary relative to C/L = 0.00 On centerline TOC below baseline = Legs on bottom

SHEET 1 - SUMMARY SHEET

SUMMARY - LOAD TABLE

Item	Weight kips	LCG feet	LM ft-kips	TCG feet	TM ft-kips	VCG feet	VM ft-kips	FSML ft-kips	FSMT ft-kips
Hull - Basic & Fixed Loads	7068.90		787118		15339		#N/A		
Cantilever Beam Loading	870.00		136755		-1523		#N/A		
Drill Floor & Equipment	580.00		107138		220		#N/A		
Legs 360.33 ft	3258.30		389173		0	#N/A	#N/A		
LIGHTWEIGHT	11777.20	_	1420184	-	14037		#N/A		
Changes to basic hull	77.30		10896		1757		#N/A		
Changes to cant. beam assembly	10.00	160.00	1600		-190		#N/A		
Changes to drill floor	11.20	196.89	2211	-17.75	-199		#N/A		
SOLID VARIABLES	1123.40	-	151524		-19851		#N/A		
LIQUID VARIABLES	1159.20		104595		4443		#N/A	#N/A	#N/A
PRELOAD	7138.40		852709		87		#N/A	#N/A	#N/A
HOOK LOAD	0.00	0.00	0	0.00	0		#N/A		_
LOADED DISPLACEMENT	21296.70		2543719		84		#N/A	#N/A	#N/A
CG Location		119.44		0.00		#N/A			

	STABILITY & LEG REACTION SUMMARY										
	AFLOAT S	ABILITY LEG REACTIO	LEG REACTIONS								
HYDRO DATA		TRIM & LIST									
Draft (feet) LCB (feet) KML (feet) KMT (feet)	#N/A #N/A #N/A #N/A	Trim#N/AdegBOW LEG ReactionTrim#N/AfeetSTBD LEG ReactionList#N/AdegPORT LEG ReactionList#N/Afeet	7099 7100 7098	kips kips kips							
STAB DATA		DRAFTS Water depth	250	feet							
KGmax 70 Kts (feet) KGmax 100 Kts (feet) FSCL (feet)	#N/A #N/A #N/A	Stbd-Fwd #N/A feet Port-Fwd #N/A feet Stbd-Aft #N/A feet	21297 2381	kips kips							
FSCT (feet) KGL (feet) KGT (feet) GML (feet)	#N/A #N/A #N/A #N/A	Port-Aft #N/A feet VAR LOADS MARGIN	0	kips							

FORM #2 PRELOAD

SHEET 2 - SOLID VARIABLE LOADS

	Ullage	Weight	LCG	LM	TCG	TM	VCG	VM	
Item	feet	kips	feet	ft-kips	feet	ft-kips	feet	ft-kips	
Bulk tank #1 (Port)	0.00	188.10	128.00	24077	-67.00	-12603	30.50	5737	
Bulk tank #2 (Port)	5.78	133.70	128.00	17119	-53.00	-7088	28.00	3745	
Bulk tank #3 (Stbd)	6.00	68.20	128.00	8727	53.00	3614	27.50	1875	
Bulk tank #4 (Stbd)	17.35	12.90	128.00	1652	67.00	865	24.00	310	
Mud pump room		6.00	77.00	462	0.00	0	7.50	45	North Contraction
Engine room		5.00	156.00	780	0.00	0	7.50	38	
Mechanic's shop		5.00	156.00	780	30.00	150	7.50	38	
Haliburton room		0.00	131.00	0	35.00	0	0.00	0	
Mud logging unit		10.00	190.00	1900	39.00	390	41.00	410	
Port storage		10.00	67.60	676	-32.00	-320	7.00	70	
Sack room		106.00	138.00	14628	-40.00	-4240	8.50	901	
Crew and effects		18.00	78.00	1404	0.00	0	35.00	630	
Casing		0.00	126.25	0	0.00	0	0.00	0	and the second second
Misc under radiators		8.00	195.00	1560	-50.00	-400	22.00	176	
Misc		8.00	156.00	1248	-52.00	-416	22.00	176	
Paint locker & contents	5	8.00	51.00	408	-32.00	-256	23.00	184	
Storage under cantilev	er	6.00	170.00	1020	0.00	0	22.50	135	
Risers		7.00	172.00	1204	-40.00	-280	32.00	224	
Drums 22 @425 lbs		9.40	170.00	1590	-60.00	-561	21.50	201	
Misc equip @ shaker		15.00	189.00	2835	58.00	870	24.50	368	
Containers (2)		25.00	138.00	3450	40.00	1000	23.50	588	
Misc scrap		10.00	160.00	1600	52.00	520	20.00	200	
Total Port & Stbd L	oading	659.30	1. Sec. 1.	87119		-18756		16048	
Cantilever Beam Lo	ading	1							
Port pipe rack		134.60	128.00	17229	-11.75	-1582	39.00	5249	
Stbd pipe rack		89.20	128.00	11418	15.00	1338	39.00	3479	
Port drill collar rack		75.50	128.00	9664	-23.75	-1793	37.50	2831	
Stbd drill collar rack		64.80	128.00	8294	20.75	1345	37.50	2430	
Hydrill		15.00	179.00	2685	20.75	311	28.00	420	
BOPs		55.00	179.00	9845	-13.00	-715	29.00	1595	
Misc		20.00	179.00	3580	0.00	0	51.00	1020	
Subs		10.00	169.00	1690	0.00	0	36.00	360	
Total Cantilever L	oading	464.10		64405		-1096		17384	
TOTAL SOLID VAR	IABLES	1123.40		151524		-19851		33433	



SHEET 3 - LIQUID VARIABLE LOADS

	Sound	Weight	LCG	LM	TCG	TM	VCG	VM	FSML	FSMT
Tank Datable water That	teet	KIPS	feet	TT-KIPS	teet	TT-KIPS	reet	TT-KIPS	1707	IT-KIPS
Potable water - 1K4	4.58	157.80	65.30	10311	14.22	2243	2.29	361	1707	1965
Polable water - TK 5	4.30	157.00	05.30	10311	-14.22	-2243	2.29	301	1 1/07	1905
Drill water - #1	4.81	120 50	4.63	558	0.00	1 0	2.41	200	181	4580
Drill water - #6	4.81	160.70	78.30	12585	33.51	5386	2 41	387	4464	932
Drill water - #7	1.89	63.20	78.30	4945	-33.51	-2116	0.95	60	4464	932
Drill water - #10	0.61	16.00	85.30	1361	12.08	193	0.31	5	725	1345
Drill water - #11	0.61	16.00	85.30	1361	-12.08	-193	0.31	5	725	1345
Drill water - #17	0.00	0.00	126,16	0	-13.00	0	0.00	0	0	0
Drill water - #18	0.00	0.00	126,91	0	12.17	0	0.00	0	0	0
Drill water - #23	0.94	48.30	156.00	7539	-13.00	-628	0.47	23	4708	2982
Drill water - #24	0.94	48.30	156.00	7539	13.00	628	0.47	23	4708	2982
Drill water - #25	4.08	123.90	154.62	19153	-34.00	-4212	2.04	253	3045	777
Drill water - #26	1.75	53.10	154.62	8215	34.00	1806	0.88	46	3045	777
Diesel oil - #13	2.74	48.90	105.94	5184	-41.41	-2026	1.37	67	404	1034
Diesel oil - #14	5.00	122.00	104.12	12702	39.16	4777	2.50	305	0	0
Diesel oil - #19	0.00	0.00	126.37	0	-42.69	0	0.00	0	0	0
Diesel oil - #20	0.48	16.70	126.71	2110	41.20	686	0.24	4	1774	3474
Dirty oil tank	2.10	6.10	117.16	720	23.00	141	1.00	6	20	8
Mud pit #1 (Stbd)	0.00	0.00	103.66	0	19.50	0	5.00	0	0	0
Mud pit #2 (Stbd)	0.00	0.00	104.67	0	5.85	0	5.00	0	0	0
Mud pit #3 (Port)	0.00	0.00	103.66	0	-6.50	0	5.00	0	0	0
Mud pit #4 (Port)	0.00	0.00	103.66	0	-19.50	0	5.00	0	0	0
Slugging pit	0.00	0.00	97.70	0	10.25	0	5.00	0	0	0
Skimmer tank	0.00	0.00	185.00	0	54.00	0	0.00	0	0	0
Sand traps		0.00	190.00	0	40.00	0	25.00	0	0	0
TOTAL LIQUID VA	RIABLES	1159.20		104595		4443		2195	31677	25098
PRELOAD TANKS										
	Sound	Weight	LCG	LM	TCG	TM	VCG	VM	FSML	FSMT
Tank Destand Tests # 0	feet	KIPS	feet	IT-KIPS	teet	ft-kips	feet	ft-kips	ft-kips	ft-kips
Preload Tank # 2	10.69	530.20	28.89	15317	23.28	12342	5.35	2834	8768	4494
Preload Tank # 3	10.53	530.20	28.85	15298	-23.35	-12381	5.27	2792	8/65	4511
Preload Tank # 6	20.00	581.10	69.17	40191	44.46	25833	10.00	5811	0	0
Preload Tank # 9	20.00	620.60	68.17	42303	-43./1	-2/124	10.00	6206	0	0
Preload Tank #15	20.00	638.30	103.66	66164	-59.26	-3/824	10.00	6383	0	0
Preload Tank #16	20.00	638.30	103.66	66164	59.26	37824	10.00	6383	0	0
Preload Tank #21A	20.00	706.80	141.75	100189	-74.95	-52975	10.00	7068	0	0
Preload Tank #22A	20.00	720.90	141.65	102121	74.98	54056	10.00	7209	0	0
Preload Tank #218	20.00	559.20	184.06	102926	-65.02	-36359	10.00	5592	0	0
Proload Tank #228	12.00	526.40	184.05	96888	65.//	34623	10.00	5264	0	1000
Proload Tank #20	11.05	5/3.20	100.00	06005	36.10	20692	6./4	3860	3966	1600
TOTAL PRELOA	0	7109 40	108.79	90895	-30.28	-18620	5.93	3041	7328	2413
TOTAL PRELOA	0	/138.40		1 822109		8/		62442	28821	13018

COASTAL DRILLER Load Calculation Form



Rotary aft of transom = 40.00 feet Rotary relative to C/L = -8.00 feet port of centerline TOC below baseline = Legs on bottom

SHEET 1 - SUMMARY SHEET

SUMMARY - LOAD TABLE

Item	Weight	LCG	LM ft-kine	TCG	TM ft-kine	VCG	VM ft-kine	FSML ft-kine	FSMT ft-kins
Hull - Basic & Fixed Loads	7068.90	1001	787118	1001	15339	1001	#N/A	II-KIP3	пекірэ
Cantilever Beam Loading	870.00		196202		-1523		#N/A		
Drill Floor & Equipment	580.00		146769		-4420		#N/A		
Legs 360.33 ft	3258.30		389173		0	#N/A	#N/A		
LIGHTWEIGHT	11777.20		1519262		9397		#N/A	1	
Changes to basic hull	77.30		10896		1757		#N/A		
Changes to cant. beam assembly	10.00	228.33	2283		-190		#N/A		
Changes to drill floor	11.20	265.22	2978	-25.75	-289		#N/A		
SOLID VARIABLES	1029.40		144220		-17414		#N/A		
LIQUID VARIABLES	2253.10		181648		4291		#N/A	#N/A	#N/A
PRELOAD	0.00		0		0		#N/A	#N/A	#N/A
HOOK LOAD	277.80	247.33	68708	-8.00	-2222		#N/A		
	15436.00		1020007		4671		#NI/A	#NI/A	#NI/A
CG Location	10400.00	125.03	1323337	-0.30	-40/1	#N/A	#IV/A	#IVA	#IN/A

	STA	BILITY & LEG REACTION SUMMARY				
	AFLOAT S	TABILITY LEG REACTIONS	LEG REACTIONS			
HYDRO DATA		TRIM & LIST				
Draft (feet) LCB (feet) KML (feet) KMT (feet)	#N/A #N/A #N/A #N/A	Trim#N/AdegBOW LEG Reaction4436Trim#N/AfeetSTBD LEG Reaction5461List#N/AdegPORT LEG Reaction5539	kips kips kips			
STAB DATA		DRAFTS Water depth 250	feet			
KGmax 70 Kts (feet) KGmax 100 Kts (feet) FSCL (feet) FSCT (feet)	#N/A #N/A #N/A #N/A	Stbd-Fwd #N/A feet TOTAL WEIGHT 15436 Port-Fwd #N/A feet VARIABLE LOADS 3381 Stbd-Aft #N/A feet VARIABLE LOADS 3381	kips kips			
KGL (feet) KGT (feet) GML (feet) GMT (feet)	#N/A #N/A #N/A #N/A	VAR LOADS MARGIN 0	KIPS			

FORM #3 DRILLING

SHEET 2 - SOLID VARIABLE LOADS

	Ullage	Weight	LCG	LM	TCG	TM	VCG	VM	
Item	feet	kips	feet	ft-kips	feet	ft-kips	feet	ft-kips	
Bulk tank #1 (Port)	0.00	188.10	128.00	24077	-67.00	-12603	30.50	5737	
Bulk tank #2 (Port)	5.78	133.70	128.00	17119	-53.00	-7088	28.00	3745	
Bulk tank #3 (Stbd)	6.00	68.20	128.00	8727	53.00	3614	27.50	1875	
Bulk tank #4 (Stbd)	17.35	12.90	128.00	1652	67.00	865	24.00	310	
Mud pump room		6.00	77.00	462	0.00	0	7.50	45	
Engine room		5.00	156.00	780	0.00	0	7.50	38	
Mechanic's shop		5.00	156.00	780	30.00	150	7.50	38	
Halliburton room		0.00	131.00	0	35.00	0	0.00	0	
Mud logging unit		10.00	190.00	1900	39.00	390	41.00	410	
Port storage		10.00	67.60	676	-32.00	-320	7.00	70	
Sack room		106.00	138.00	14628	-40.00	-4240	8.50	901	
Crew and effects		18.00	78.00	1404	0.00	0	35.00	630	
Casing		238.80	126.25	30149	0.00	0	0.00	0	
Misc under radiators		8.00	195.00	1560	-50.00	-400	22.00	176	
Misc		8.00	156.00	1248	-52.00	-416	22.00	176	-
Paint locker & content	S	8.00	51.00	408	-32.00	-256	23.00	184	
Storage under cantilev	ver	6.00	170.00	1020	0.00	0	22.50	135	
Risers		7.00	172.00	1204	-40.00	-280	32.00	224	
Drums 22 @425 lbs		9.40	170.00	1590	-60.00	-561	21.50	201	
Misc equip @ shaker		15.00	189.00	2835	58.00	870	24.50	368	
Containers (2)		25.00	138.00	3450	40.00	1000	23.50	588	
Misc scrap		10.00	160.00	1600	52.00	520	20.00	200	
Total Port & Stbd L	oading	898.10		117267		-18756		16048	
Port pipe rack	oading	8.20	196.33	1610	-11.75	-96	39.00	320	
Stbd pipe rack		89.20	196.33	17513	15.00	1338	39.00	3479	
Port drill collar rack		8,90	196.33	1747	-23.75	-211	37.50	334	
Stbd drill collar rack		0.00	196.33	0	20.75	0	37.50	0	
Hydrill		15.00	247.33	3710	20.75	311	28.00	420	
BOPs		0.00	247.33	0	-13.00	0	29.00	0	
Misc		0.00	247.33	0	0.00	0	51.00	0	
Subs		10.00	237.33	2373	0.00	0	36.00	360	
Total Cantilever L	oading	131.30		26953		1342		4912	
TOTAL SOLID VAR	RIABLES	1029,40		144220		-17414		20961	
						1		20001	



SHEET 3 - LIQUID VARIABLE LOADS

	Sound	Weight	LCG	LM	TCG	TM	VCG	VM	FSML	FSMT
Tank Detektor That	teet	KIPS	reet	TT-KIPS	14.00	IT-KIPS	1eet	261	1707	1065
Potable water - 1k 4	4.58	157.80	65.36	10311	14.22	2243	2.29	361	1707	1965
Potable water - 1K5	4.58	157.80	65.36	10311	-14.22	-2243	2.29	301	1707	1905
Drillwator #1	1 18 00	451.00	4.63	2088	0.00		9.00	4059	181	4580
Drill water - #1	5.00	167.10	78 30	13082	33.51	5500	2.50	418	0	0
Drill water - #7	1.67	156.10	78.30	12219	-33.51	-5229	2.34	364	4464	932
Drill water - #10	3.00	78.40	85.30	6691	12.08	948	1.50	118	725	1345
Drill water - #10	1.58	119.80	85.30	10215	-12.08	-1447	2.29	274	725	1345
Drill water - #17	2.00	85.00	126.16	10721	-13.00	-1105	1.00	85	2659	2464
Drill water - #18	2.00	97.30	126.10	12345	12 17	1184	1.24	121	2340	2090
Drill water - #23	0.50	25.70	156.00	4010	-13.00	-334	0.25	6	4708	2982
Drill water - #24	0.50	25.70	156.00	4010	13.00	334	0.25	6	4708	2982
Drill water - #25	0.50	15.20	154.62	2347	-34.00	-516	0.25	4	3045	777
Drill water - #26	0.00	0.00	154.62	0	34.00	0	0.00	0	0	0
Dilli Water - #20	0.00	0.00	104.02		04.00		0.00			<u> </u>
Diesel oil - #13	2 75	49 10	105 94	5203	-41.41	-2034	1.38	68	404	1034
Diesel oil - #14	5.00	122.00	104 12	12702	39.16	4777	2.50	305	0	0
Diesel oil - #19	0.50	23.40	126.37	2952	-42.69	-997	0.25	6	2870	4485
Diesel oil - #20	0.00	0.00	126.71	0	41.20	0	0.00	0	0	0
Dirty oil tank	2.00	5.90	117 16	686	23.00	135	1.00	6	20	8
Dirty Oil tarik	2.00	0.00	117.10	1 000	20.00	1 100	1.00		20	
Mud pit #1 (Stbd)	5.00	96.20	103.66	9970	19.50	1875	7.50	721	633	328
Mud pit #2 (Stbd)	5.00	82.00	104.67	8588	5.85	480	7.50	615	481	263
Mud pit #3 (Port)	6.50	121.70	103.66	12611	-6.50	-791	8.25	1004	633	328
Mud pit #4 (Port)	6.50	121.70	103.66	12611	-19.50	-2372	8.25	1004	633	328
Slugging pit	0.00	0.00	97.70	0	10.25	0	5.00	0	0	0
Skimmer tank	0.00	0.00	185.00	0	54.00	0	0.00	0	0	0
Sand traps		94.60	190.00	17974	40.00	3784	25.00	2365	0	0
TOTAL LIQUID VA	RIABLES	2253.10		181648		4291		12271	32643	30201
PRELOAD TANKS										
	Sound	Weight	LCG	LM	TCG	TM	VCG	VM	FSML	FSMT
Tank	feet	kips	feet	ft-kips	feet	ft-kips	feet	ft-kips	ft-kips	ft-kips
Preload Tank # 2	0.00	0.00	28.89	0	23.28	0	0.00	0	0	0
Preload Tank # 3	0.00	0.00	28.85	0	-23.35	0	0.00	0	0	0
Preload Tank # 8	0.00	0.00	69.17	0	44.46	0	0.00	0	0	0
Preload Tank # 9	0.00	0.00	68.17	0	-43.71	0	0.00	0	0	0
Preload Tank #15	0.00	0.00	103.66	0	-59.26	0	0.00	0	0	0
Preload Tank #16	0.00	0.00	103.66	0	59.26	0	0.00	0	0	0
Preload Tank #21A	0.00	0.00	141.75	0	-74.95	0	0.00	0	0	0
Preload Tank #22A	0.00	0.00	141.65	0	74.98	0	0.00	0	0	0
Preload Tank #21B	0.00	0.00	184.06	0	-65.02	0	0.00	0	0	0
Preload Tank #22B	0.00	0.00	184.05	0	65.77	0	0.00	0	0	0
Preload Tank #28	0.00	0.00	188.86	0	36.10	0	0.00	0	0	0
Preload Tank #29	0.00	0.00	188.79	0	-36.28	0	0.00	0	0	0
TOTAL PRE	LOAD	0.00		0		0		0	0	0

COASTAL DRILLER Load Calculation Form



Rotary fwd of transom = 28.33 feet Rotary relative to C/L = 0.00 feet TOC below baseline = Legs on bottom

SHEET 1 - SUMMARY SHEET

SUMMARY - LOAD TABLE

Item	Weight	LCG	LM ft-kine	TCG	TM	VCG	VM ft-kins	FSML ft-kins	FSMT ft-kins
Hull - Basic & Fixed Loads	7068.90	Idet	787118	1001	15339		#N/A	TERIPS	ICRIPS
						-			
Cantilever Beam Loading	870.00		136755		-1523		#N/A		
Drill Floor & Equipment	580.00		107138		220		#N/A		
Legs 360.33 ft	3258.30		389173		0	#N/A	#N/A		
LIGHTWEIGHT	11777.20		1420184	-	14037		#N/A		
Changes to basic hull	77.30		10896		1757		#N/A		
Changes to cant. beam assembly	10.00	160.00	1600	1	-190		#N/A		
Changes to drill floor	11.20	196.89	2211	-17.75	-199		#N/A		
SOLID VARIABLES	1123.40		151524		-19851		#N/A		
LIQUID VARIABLES	1159.20		104595		4443		#N/A	#N/A	#N/A
PRELOAD	0.00		0		0		#N/A	#N/A	#N/A
HOOK LOAD	0.00	0.00	0	0.00	0		#N/A		
LOADED DISPLACEMENT	14158.30		1691010		-4		#N/A	#N/A	#N/A
CG Location		119.44		0.00		#N/A			

	STA	BILITY & LEG	REAC	CTION	SUMMARY	
	AFLOAT S	LEG REACTIONS				
HYDRO DATA	TRIM 8	LIST				
Draft (feet) LCB (feet) KML (feet) KMT (feet)	#N/A #N/A #N/A #N/A	Trim # Trim # List # List #	N/A N/A N/A N/A	deg feet deg feet	BOW LEG Reaction4720STBD LEG Reaction4719PORT LEG Reaction4719) kips) kips) kips
STAB DATA	Value Adda an Ione	DRA	FTS	_	Water depth 250) feet
KGmax 70 Kts (feet) KGmax 100 Kts (feet) FSCL (feet) FSCT (feet)	#N/A #N/A #N/A #N/A	Stbd-Fwd Port-Fwd Stbd-Aft Port-Aft	#N/A #N/A #N/A #N/A	feet feet feet feet	TOTAL WEIGHT1415VARIABLE LOADS238VAR LOADS MARGIN	8 kips 1 kips 0 kips
KGL (feet) KGT (feet) GML (feet) GMT (feet)	#N/A #N/A #N/A #N/A					

FORM #4 STORM

SHEET 2 - SOLID VARIABLE LOADS

UII	age	Weight	LCG	LM	TCG	TM	VCG	VM	
Item fe	eet	kips	feet	ft-kips	feet	ft-kips	feet	ft-kips	
Bulk tank #1 (Port) 0.	.00	188.10	128.00	24077	-67.00	-12603	30.50	5737	
Bulk tank #2 (Port) 5.	.78	133.70	128.00	17119	-53.00	-7088	28.00	3745	
Bulk tank #3 (Stbd) 6.	.00	68.20	128.00	8727	53.00	3614	27.50	1875	
Bulk tank #4 (Stbd) 17	7.35	12.90	128.00	1652	67.00	865	24.00	310	
Mud pump room		6.00	77.00	462	0.00	0	7.50	45	
Engine room		5.00	156.00	780	0.00	0	7.50	38	
Mechanic's shop		5.00	156.00	780	30.00	150	7.50	38	
Haliburton room		0.00	131.00	0	35.00	0	0.00	0	
Mud logging unit		10.00	190.00	1900	39.00	390	41.00	410	
Port storage		10.00	67.60	676	-32.00	-320	7.00	70	
Sack room		106.00	138.00	14628	-40.00	-4240	8.50	901	
Crew and effects		18.00	78.00	1404	0.00	0	35.00	630	
Casing		0.00	126.25	0	0.00	0	0.00	0	
Misc under radiators		8.00	195.00	1560	-50.00	-400	22.00	176	
Misc		8.00	156.00	1248	-52.00	-416	22.00	176	
Paint locker & contents		8.00	51.00	408	-32.00	-256	23.00	184	
Storage under cantilever		6.00	170.00	1020	0.00	0	22.50	135	
Risers		7.00	172.00	1204	-40.00	-280	32.00	224	
Drums 22 @425 lbs		9.40	170.00	1590	-60.00	-561	21.50	201	
Misc equip @ shaker		15.00	189.00	2835	58.00	870	24.50	368	
Containers (2)		25.00	138.00	3450	40.00	1000	23.50	588	
Misc scrap		10.00	160.00	1600	52.00	520	20.00	200	
Total Port & Stbd Loa	ading	659.30		87119		-18756		16048	
Cantilever Beam Loadi	ing	- Anna an							
Port pipe rack		134.60	128.00	17229	-11.75	-1582	39.00	5249	
Stbd pipe rack		89.20	128.00	11418	15.00	1338	39.00	3479	
Port drill collar rack		75.50	128.00	9664	-23.75	-1793	37.50	2831	
Stbd drill collar rack		64.80	128.00	8294	20.75	1345	37.50	2430	
Hydrill		15.00	179.00	2685	20.75	311	28.00	420	
BOPs		55.00	179.00	9845	-13.00	-715	29.00	1595	
Misc		20.00	179.00	3580	0.00	0	51.00	1020	
Subs		10.00	169.00	1690	0.00	0	36.00	360	
Total Cantilever Loadi	ing	464.10		64405		-1096		17384	
TOTAL SOLID VARIAE	BLES	1123.40		151524		-19851		33433	



SHEET 3 - LIQUID VARIABLE LOADS

Taula	Sound	Weight	LCG	LM	TCG	TM	VCG	VM	FSML	FSMT
	teet	KIPS	teet	TT-KIPS	reet	ft-kips	reet	IT-KIPS	IT-KIPS	TT-KIPS
Potable water - 1k 4	4.58	157.80	65.36	10311	14.22	2243	2.29	361	1707	1965
Folable water - TK 5	4.30	157.60	05.30	10311	-14.22	-2243	2.29	301	1707	1905
Drill water - #1	4.81	120.50	4.63	558	0.00		2.41	200	181	4580
Drill water - #6	4.01	160.70	78.30	12585	33.51	5386	2.41	387	4464	932
Drill water - #7	1.89	63.20	78.30	4945	-33.51	-2116	0.95	60	4464	932
Drill water - #10	0.61	16.00	85.30	1361	12.08	193	0.31	5	725	1345
Drill water - #11	0.61	16.00	85.30	1361	-12.08	-193	0.31	5	725	1345
Drill water - #17	0.00	0.00	126.16	0	-13.00	0	0.00	0	0	0
Drill water - #18	0.00	0.00	126.91	0	12.17	0	0.00	0	0	0
Drill water - #23	0.94	48.30	156.00	7539	-13.00	-628	0.47	23	4708	2982
Drill water - #24	0.94	48.30	156.00	7539	13.00	628	0.47	23	4708	2982
Drill water - #25	4.08	123.90	154.62	19153	-34.00	-4212	2.04	253	3045	777
Drill water - #26	1.75	53.10	154.62	8215	34.00	1806	0.88	46	3045	777
	1			1		1 ,000				
Diesel oil - #13	2.74	48.90	105.94	5184	-41.41	-2026	1.37	67	404	1034
Diesel oil - #14	5.00	122.00	104.12	12702	39,16	4777	2.50	305	0	0
Diesel oil - #19	0.00	0.00	126.37	0	-42.69	0	0.00	0	0	C
Diesel oil - #20	0.48	16.70	126.71	2110	41.20	686	0.24	4	1774	3474
Dirty oil tank	2.10	6.10	117.16	720	23.00	141	1.00	6	20	8
						1				
Mud pit #1 (Stbd)	0.00	0.00	103.66	0	19.50	0	5.00	0	0	0
Mud pit #2 (Stbd)	0.00	0.00	104.67	0	5.85	0	5.00	0	0	0
Mud pit #3 (Port)	0.00	0.00	103.66	0	-6.50	0	5.00	0	0	0
Mud pit #4 (Port)	0.00	0.00	103.66	0	-19.50	0	5.00	0	0	0
Slugging pit	0.00	0.00	97.70	0	10.25	0	5.00	0	0	0
Skimmer tank	0.00	0.00	185.00	0	54.00	0	0.00	0	0	0
Sand traps		0.00	190.00	0	40.00	0	25.00	0	0	0
TOTAL LIQUID VA	RIABLES	1159.20		104595		4443		2195	31677	25098
								A	A	Annual and the second second
PRELOAD TANKS										
101-101-101-101-101-101-101-101-101-101	Sound	Weight	LCG	LM	TCG	TM	VCG	VM	FSML	FSMT
Tank	feet	kips	feet	ft-kips	feet	ft-kips	feet	ft-kips	ft-kips	ft-kips
Preload Tank # 2	0.00	0.00	28.89	0	23.28	0	0.00	0	0	0
Preload Tank # 3	0.00	0.00	28.85	0	-23.35	0	0.00	0	0	0
Preload Tank # 8	0.00	0.00	69.17	0	44.46	0	0.00	0	0	0
Preload Tank # 9	0.00	0.00	68.17	0	-43.71	0	0.00	0	0	0
Preload Tank #15	0.00	0.00	103.66	0	-59.26	0	0.00	0	0	0
Preload Tank #16	0.00	0.00	103.66	0	59.26	0	0.00	0	0	0
Preload Tank #21A	0.00	0.00	141.75	0	-74.95	0	0.00	0	0	0
Preload Tank #22A	0.00	0.00	141.65	0	74.98	0	0.00	0	0	0
Preload Tank #21B	0.00	0.00	184.06	0	-65.02	0	0.00	0	0	0
Preload Tank #22B	0.00	0.00	184.05	0	65.77	0	0.00	0	0	0
Preload Tank #28	0.00	0.00	188.86	0	36.10	0	0.00	0	0	0
Preload Tank #29	0.00	0.00	188.79	0	-36.28	0	0.00	0	0	0
TOTAL PRELOAD		0.00		0		0		0	0	0

CHAPTER 5 - OPERATING DATA

1. Hydrostatic tables

(Pages 5-4 and 5-5)

Abbreviations used in the hydrostatic tables:

- LCB Longitudinal location of the Center of Buoyancy, measured in feet aft of frame zero (AF0). The Center of Buoyancy is located at the geometric center of the underwater volume.
- LCF Longitudinal location of the Center of Flotation, measured in feet aft of frame zero (AF0). The Center of Flotation is located at the geometric center of the waterplane area.
- **KM** Height of the metacenter measured in feet above the keel. Metacenter may be longitudinal (L) or transverse (T).

- **KB** Vertical height of the Center of Buoyancy measured in feet above the baseline (keel). KB is located at half-draft.
- **BM** Metacentric Radius; the vertical distance in feet between the Center of Buoyancy and the Metacenter. The metacenter may be longitudinal (L) or transverse (T).

$$BML = \frac{Jr}{V} \qquad BMT = \frac{J}{V}$$

- I Moment of Inertia of the waterplane area about axis through the Center of Flotation. Longitudinal = 53,900,752 ft⁴; transverse = 28,527,995 ft⁴.
- V Displacement volume.
- **KPI** The load change in kips which results in a draft change of one inch.

2. Maximum allowable KG

Two curves provide the maximum allowed KG for a specific draft depending on the mode of operation and wind speed (70 or 100 knots).

Stability is acceptable if neither the KGL nor the KGT, obtained through the load form calculations, exceeds the value shown on the curves.

3. Design limits of legs (afloat)

(Page 5-7)

The motions of the jackup during a normal transit when wind speeds are less than 70 knots are limited by leg strength as shown on the upper curve (B) of the Design Limits of Legs (Afloat) Graph. The jack-up may be in a field or ocean transit. In either case, the TOC should be the proper distance (1.2 feet for field transit and 12.38 feet for ocean transit) below the hull.

In weather conditions in which the expected winds exceed 70 knots, the legs must be lowered so that the spud can tips must be lowered to 60.50 feet below the hull in order to meet the stability and leg strength requirements defined by curve A of the Design Limits of Legs (Afloat) Graph.

4. Safe motion for going on location

(Page 5-8)

For the appropriate water depth, enter the chart with the observed inclination in degrees and the period for the motion. The observed inclination for pitch, roll, or combined pitch-roll is the angle from level to maximum inclination. This is the maximum angle read from the control room inclinometers. The period is timed for a complete cycle. For example: the period in seconds between successive instances of maximum port side down. Any combination of angle and period which lies below the appropriate water depth curve is considered acceptable.

5. Allowable wind and wave charts

(Pages 5-9 through 5-20)

These charts give the various combinations of wind, waves, and current in which elevated operations are permitted for a given leg reaction and water depth.

The following data must be available to use the charts:

- The largest of the three leg reactions.
- The amount of leg penetration. If the penetration exceeds 25 feet, the water depth value must be increased by the amount of additional penetration.
- Water depth including astronomical and storm tides.

The procedures for using the charts are as follows:

- (1) Select the appropriate chart based on leg length, minimum air gap, water depth, and current for the particular site in question. For water depths and current velocities that fall between charts, use the chart with the next highest values.
- (2) At the "highest leg reaction" calculated value, read across the chart to determine wave height and wind speed combinations which are permitted.
- (3) Compare the actual or predicted wind and wave values to those shown in the Allowable Wind and Wave Chart. If they are less than the allowable, the unit is in a satisfactory condition.

6. Limits of Service

(Page 5-21)

(Page 5-22)

The limits of service for afloat and elevated conditions show the configuration necessary to withstand winds greater than 70 knots.

7. Cantilever beam loading chart

The Cantilever Beam Load Charts show the limits in the drilling loads (hook, rotary, setback, and conductor tension). Any increase in drill package weight and centers of gravity specified in the basic weight will cause an equivalent decrease in the allowable drilling loads.

8. Changes to Lightweight

Changes to lightweight for the Coastal Driller which have taken place since the original inclining experiment (10/15/82) are shown in the formal record: Changes to Lightweight.

The weights and moments shown in the record will be treated as a variable load until a change to lightweight has been approved.

(Page 5-23)

Draft	Displacement	LCB	LCF	KML	KMT	KPI
ft-in	Kips	ft	ft	ft	ft	kips/in
70	9107.68	119.44	119.44	382.26	203.97	108.43
1	9216.11	119.44	119.44	377.85	201.65	108.43
2	9324.53	119.44	119.44	373.54	199.39	108.43
3	9432.96	119.44	119.44	369.33	197.18	108.43
4	9541.38	119.44	119.44	365.21	195.02	108.43
5	9649.81	119.44	119.44	361.19	192.91	108.43
6	9758.23	119.44	119.44	357.26	190.85	108.43
7	9866.66	119.44	119.44	353.42	188.84	108.43
8	9975.08	119.44	119.44	349.66	186.87	108.43
9	10083.51	119.44	119.44	345.98	184.94	108.43
10	10191.93	119.44	119.44	342.39	183.06	108.43
11	10300.36	119.44	119.44	338.86	181.21	108.43
8 0	10408.78	119.44	119.44	335.42	179.41	108.43
1	10517.21	119.44	119.44	332.04	177.64	108.43
2	10625.63	119.44	119.44	328.74	175.91	108,43
3	10734.06	119.44	119.44	325.50	174.22	108.43
4	10842.48	119.44	119.44	322.33	172.56	108.43
5	10950.91	119.44	119.44	319.22	170.93	108.43
6	11059.33	119.44	119.44	316.17	169.34	108.43
7	11167.76	119.44	119.44	313.19	167.78	108.43
8	11276.18	119.44	119.44	310.26	166.25	108.43
9	11384.61	119.44	119.44	307.38	164.75	108.43
10	11493.03	119.44	119.44	304.57	163.28	108.43
11	11601.46	119.44	119.44	301.80	161.83	108.43
90	11709.88	119.44	119.44	299.09	160.42	108.43
1	11818.31	119.44	119.44	296.43	159.03	108.43
2	11926.73	119.44	119.44	293.82	157.67	108.43
3	12035.16	119.44	119.44	291.26	156.33	108.43
4	12143.58	119.44	119.44	288.74	155.02	108.43
5	12252.01	119.44	119.44	286.27	153.73	108.43
6	12360.43	119.44	119.44	283.84	152.46	108.43
7	12468.86	119.44	119.44	281.45	151.22	108.43
8	12577.28	119.44	119.44	279.11	150.00	108 43
9	12685.71	119.44	119.44	276.81	148 80	108.43
10	12794.13	119.44	119.44	274.54	147 62	108.43
11	12902 56	119 44	119.44	272 32	146 46	108.43

TABLE OF HYDROSTATIC PROPERTIES COASTAL DRILLER

Continued on next page.

Draft	Displacement	LCB	LCF	KML	KMT	KPI kipg/ip
11-111	rips	11	n	IL	IL	KIPS/III
10 0	13010.98	119.44	119.44	270.13	145.33	108.43
1	13119.41	119.44	119.44	267.98	144.21	108.43
2	13227.83	119.44	119.44	265.87	143.11	108.43
3	13336.26	119.44	119.44	263.79	142.03	108.43
4	13444.68	119.44	119.44	261.75	140.97	108.43
5	13553.11	119.44	119.44	259.74	139.92	108.43
6	13661.53	119.44	119.44	257.76	138.89	108.43
7	13769.96	119.44	119.44	255.81	137.88	108.43
8	13878.38	119.44	119.44	253.90	136.89	108.43
9	13986.81	119.44	119.44	252.01	135.91	108.43
10	14095.23	119.44	119.44	250.16	134.95	108.43
11	14203.66	119.44	119.44	248.33	134.00	108.43
11 0	14312.08	119.44	119.44	246.53	133.07	108.43
1	14420.51	119.44	119.44	244.76	132.15	108.43
2	14528.93	119.44	119.44	243.02	131.25	108.43
3	14637.36	119.44	119.44	241.30	130.36	108.43
4	14745.78	119.44	119.44	239.61	129.48	108.43
5	14854.21	119.44	119.44	237.94	128.62	108.43
6	14962.63	119.44	119.44	236.30	127.77	108.43
7	15071.06	119.44	119.44	234.68	126.94	108.43
8	15179.48	119.44	119.44	233.09	126.11	108.43
9	15287.91	119.44	119.44	231.52	125.30	108.43
10	15396.33	119.44	119.44	229.97	124.50	108.43
11	15504.76	119.44	119.44	228.45	123.72	108.43
12 0	15613.18	119.44	119.44	226.94	122.94	108.43
COASTAL DRILLER MAXIMUM ALLOWABLE KG









70

32 FT AIR GAP 5' wave height ~25' 10' 15' /30' 20' -35 MAXIMUM LEG REACTION (KIPS) -40' 5900 -WIND SPEEDS (KNOTS) 5-10

150 FT WATER DEPTH 0 KNOT CURRENT



200 FT WATER DEPTH 0 KNOT CURRENT 30 FT AIR GAP

250 FT WATER DEPTH 0 KNOT CURRENT 25 FT AIR GAP





100 FT WATER DEPTH 1 KNOT CURRENT 35 FT AIR GAP

150 FT WATER DEPTH 1 KNOT CURRENT 32 FT AIR GAP





250 FT WATER DEPTH 1 KNOT CURRENT 25 FT AIR GAP



100 FT WATER DEPTH 2 KNOT CURRENT





150 FT WATER DEPTH 2 KNOT CURRENT 32 FT AIR GAP



250 FT WATER DEPTH 2 KNOT CURRENT 25 FT AIR GAP



LIMITS OF SERVICE Coastal Driller

LIMITS OF SERVICE AFLOAT See page 2-6					
Condition	Max Draft	Wind Speed	тос	Max KG	
Normal	10.88	70	1.20	65.00	
Ocean Tow	10.88	70	12.38	65.00	
Storm	10.88	100	60.50	38.75	

LIMITS OF SERVICE ELEVATED See page 3-10 Wind velocity = 100 knots Wave period = 12 seconds				
Water Depth (feet)	Air Gap (feet)	Wave Height (feet)	Surface Current (knots)	
100	35	40 37 34	0 1 2	
150	32	46 43 40	0 1 2	
200	30	42 39 36	0 1 2	
250	25	38 34 30	0 1 2	

COASTAL DRILLER CANTILEVER BEAM LOADING CHART

NOTE: Allowable drilling loads indicated are the sum of setback, hook and rotary loads in kips based on the drill package weight and center of gravity specified in the basic weight section of this operating manual.



Within the limits above, the maximum component loadings are:

HOOK LOAD	1000 kips
ROTARY LOAD	750 kips
SETBACK	450 kips

COASTAL DRILLER - CHANGES TO LIGHTWEIGHT

	Weight kips	LCG ft	LM ftkips	TCG ft	TM ftkips	VCG ft	VM ftkips
Lightship (10/15/82)	11777.18	1.	420184		14037		611010
11/18/85							
Fuel Oil Day Tank (70% Full)	12.76	123.50	1576	-22.50	- 287	14.00	179
Lube Oil Day Tank (60% Full)	5.37	126.25	678	23.00	124	13.75	74
Mud Pump Lube Oil Tank (60% Full)	5.37	56.50	303	-27.00	- 145	13.00	70
2/1/87							
Grating in Bow Leg Well P&S	8.00	30.00	240	0.00	0	19.50	156
Grating in Stbd Leg Well - Aft	4.00	176.50	706	60.00	240	19.50	78
Grating in Stbd Leg Well - Outbd	4.00	154.00	616	72.00	288	19.50	78
Grating in Port Leg Well - Aft	4.00	176.50	706	-60.00	- 240	19.50	78
Add Extra Hold-Down Claw	4.00	201.00	804	0.00	0	21.25	85
Add Port Crane Control Platform	1.50	92.00	138	-60.00	- 90	35.00	53
Add Welder's Hut and Workbench	1.50	30.00	45	10.00	15	22.00	33
Add Desander Platform	4.00	190.00	760	60.00	240	26.50	106
Remove Trip Tank (To Cantilever)	- 8.00	185.00	-1480	0.00	0	23.00	- <mark>184</mark>
1/21/88							
Add Derrick Platform & Piping	26.01	189.00	4916	58.00	1509	27.74	722
Raise Shakers & Walkways	8.81	187.00	1647	39.00	344	28.87	254
Remove Desander Platform	-4.00	190.00	-760	60.00	- 240	26.50	-106
TOTAL CHANGES TO BASIC HULL	77.32		10896		1757		1675
Add Trip Tanks and Supports	10.00	160.00	1600	-19.00	-190	28.00	280
TOTAL CHANGES TO CANTILEVER	R 10.00		1600	gadine.	-190		280
Add Water in Brake Cooling Tank	11.23	196.89	2211	-17.75	-199	35.61	400
TOTAL CHANGES IN DRILL FLOOP	11.23		2211		-199		400
TOTAL LIGHTSHIP CHANGES	98.55		14707	,	1367		2355

LEG REACTION CALCULATION FORM

Given: Weight = ______ kips LCG = ______ ft AF0 TCG = ______ ft port/stbd from CL Bow Leg Reaction = $\frac{W(160 - LCG)}{121.67}$ = ______ (160 - ____) = _____ kips Starboard Leg Reaction = $\frac{W(60 + TCG) - (Bow \times 60)}{120}$ = _____ (60 + ____) - (_____ x 60) 120 = _____ kips Port Leg Reaction = $\frac{W(60 - TCG) - (Bow \times 60)}{120}$ = _____ kips

PRELOAD CALCULATION SHEET Coastal Driller

		We	eight	LM	
P	reloaded	21,2	297.0	2,543,946	
C	ore Tanks	- 4,9	991.5	- 616,946	
D	visplacement		<u> </u>		
N	eed		the phase	<u></u>	
	Wt Fwd	=	<u>(188.82 x Wt Nee</u> 159.	ded – LM Neede 95	ed)
		=	(<u>188.82 x</u>	95)
			kips		
	Wt Aft	= .	Wt Needed – Wt F	Fwd	
		=			
		=	kips		
Tank 2	Weight		0.5 x Wt Fwd	=	_ kips
	Sounding	=	Weight/49.596	=	ft
Tank 3	Weight	=	0.5 x Wt Fwd	=	_ kips
	Sounding	=	Weight/50.356	=	_ ft
Tank 28	Weight	=	0.5 x Wt Aft + 29	=	_ kips
	Sounding	=	Weight/42.554	=	ft
Tank 29	Weight	=	0.5 x Wt Aft - 29	=	_ kips
	Sounding	=	Weight/43.314	=	ft









CHAPTER 6 - TANK CAPACITY TABLES

Tanks which are part of the hull are provided for storage of preload, potable water, drill water, and fuel oil. Active mud pits are also part of the hull. P-tanks are provided on the main deck for bulk mud and cement and are part of the fixed weight. Refer to the following tank tables for weight capacities, center of gravity locations, and free surface moments.

1. Densities used:

Drill water	62.40 lbs/cuft
Potable water	62.40 lbs/cuft
Sea water	64.00 lbs/cuft
Fuel oil	54.00 lbs/cuft
Lube oil	54.00 lbs/cuft
Drilling mud	100.00 lbs/cuft (Approx. 13.4 lbs/gal mud)

2. Free surface moments shown in the tank tables were calculated using the following formulas:

$$FSML = \frac{L^{3} B}{12000} \times p_{T}$$
$$FSMT = \frac{L B^{3}}{12000} \times p_{T}$$

where p_{τ} is the density of the liquid in the tank. See Section 1, above.

- 3. Reference axis and signs
 - LCG: (+) Aft of the bow
 - TCG: (+) Starboard of hull centerline (-) Port of hull centerline
 - VCG: (+) Above hull baseline (keel)
- 4. Weight of mud to be added to the load form:

The weight in kips in each of the mud pits shown in the mud pit tables is based on a mud density of 100.00 lbs per cubic feet. This equates to a mud weight of 13.368 lbs per gallon. The kips may be adjusted for the actual mud weight used using the following equation:

Actual Weight in kips = Weight from table x Actual mud weight 13.368

- **Example:** Compute the actual weight in mud pit 1S for a sounding level of 5.0 feet and an actual mud weight of 17.0 lbs per gallon.
- Solution: The mud pit 1S table shows a weight of 115.83 kips for a sounding of 5.0 feet. The weight is adjusted as follows:

Actual Weight = $\frac{17.0}{13.368}$ x 115.83 = 147.30 kips

TANK CAPACITY TABLES

4. Tank Tables Summary:

Tanl	kLiquid	Depth	Volume	Barrels	Weight	LCG	TCG	VCG
#	Content	feet	cuft	bbls	kips	ft	ft	ft
********		******						
1	Drill water	20.00	8029.81	1430.11	501.06	4.63	0.00	10.00
2	Preload	20.00	15498.58	2760.30	991.91	28.89	23.28	10.00
3	Preload	20.00	15726.22	2802.62	1007.12	28.85	- 23.35	10.00
4	Potable water	5.00	2760.14	491.58	172.23	65.35	14.22	2.50
5	Potable water	5.00	2760.14	491.58	172.23	65.35	- 14.22	2.50
6	Drill water	5.00	2677.64	476.89	167.08	78.30	33.51	2.50
7	Drill water	5.00	2677.64	476.89	167.08	78.30	- 33.51	2.50
8	Preload	20.00	9078.87	1616.95	581.05	69.17	44.46	10.00
9	Preload	20.00	9696.09	1726.87	620.55	68.17	- 43.71	10.00
10	Drill water	5.00	2095.20	373.16	130.74	85.30	12.08	2.50
11	Drill water	5.00	2095.20	373.16	130.74	85.30	- 12.08	2.50
13	Diesel fuel	5.00	1669.17	297.28	89.30	105.94	- 41.41	2.50
14	Diesel fuel	5.00	2280.27	406.12	121.99	104.12	39.16	2.50
15	Preload	20.00	9973.14	1776.22	638.28	103.66	- 59.26	10.00
16	Preload	20.00	9973.14	1776.22	638.28	103.66	59.26	10.00
17	Drill water	5.00	3404.70	606.38	212.45	126.16	- 13.00	2.50
18	Drill water	5.00	3142.80	559.73	196.11	126.91	12.17	2.50
19	Diesel fuel	5.00	4366.31	777.64	233.60	126.37	- 42.69	2.50
20	Diesel fuel	5.00	3242.75	577.53	173.49	126.71	41.20	2.50
21A	Preload	20.00	11043.73	1966.89	706.80	141.75	- 74.35	10.00
21B	Preload	20.00	8737.47	1556.14	559.20	184.06	- 65.02	10.00
22A	Preload	20.00	11264.62	2006.23	720.94	141.65	74.98	10.00
22B	Preload	20.00	8225.36	1464.94	526.42	184.04	65.77	10.00
23	Drill water	5.00	4119.69	733.72	257.07	156.00	- 13.00	2.50
24	Drill water	5.00	4119.69	733.72	257.07	156.00	13.00	2.50
25	Drill water	5.00	2432.63	433.25	151.80	154.62	- 34.00	2.50
26	Drill water	5.00	2432.63	433.25	151.80	154.62	34.00	2.50
28	Preload	20.00	13298.03	2368.38	851.07	188.36	36.10	10.00
29	Preload	20.00	13535.68	2410.70	866.23	188.79	- 36.28	10.00
31	Dirty oil	5.00	261.90	46.64	14.64	117.16	23.00	2.50
	Skim tank	18.63	526.77	93.82	32.87	185.00	54.00	9.31
	MudPit 1S	8.00	1853.28	330.07	185.33	103.66	19.50	9.00
	MudPit 2S	8.00	1581.03	281.58	158.10	104.67	5.85	9.00
	MudPit 3P	8.00	1853.28	330.07	185.33	103.66	- 6.50	9.00
	MudPit 4P	8.00	1853.28	330.07	185.33	103.66	- 19.50	9.00
	Slugging Pit	8.00	272.25	48.49	27.23	97.70	10.25	9.00

COASTAL DRILLER **DRILL WATER TANK 1**

LC TC	G 4.63 G 0.00	ft ft	FSML 181 FSMT 4580	ft-kips ft-kips	
Sounding ft			Weight kips	v	CG ft
0.50	*****	*****	12 53	0	25
1.00			25.05	0	50
1.50			37.58	0	75
2.00			50.11	1	00
2.50			62.63	1	25
3.00			75.16	1	.50
3.50			87.69	1	75
4.00			100.21	2	.00
4.50			112.74	2	.25
5.00			125.27	2	.50
5.50			137.79	2	.75
6.00			150.32	3	.00
6.50			162.84	3.	.25
7.00			175.37	3.	.50
7.50			187.90	3.	.75
8.00			200.42	4	.00
8.50			212.95	4	.25
9.00			225.48	4.	.50
9.50			238.00	4.	75
10.00			250.53	5.	.00
10.50			263.06	5.	.25
11.00			275.58	5.	.50
11.50			288.11	5.	.75
12.00			300.64	6	.00
12.50			313.16	6.	.25
13.00			325.69	6.	.50
13.50			338.22	6.	.75
14.00			350.74	7.	.00
14.50			363.27	1.	25
15.00			375.80	1.	50
15.50			388.32	1.	.75
16.00			400.85	8.	00
17.00			413.37	8.	20
17.50			420.90	0	75
18.00			450.45	0	00
18 50			463.48	9	25
19 00			476.01	9	50
19.50			488 53	9	75
20.00			501.06	10	00

COASTAL DRILLER PRELOAD TANK 2

LCG TCG	28.89 ft 23.28 ft		FSML 8768 ft-kips FSMT 4494 ft-kips
	Sounding ft	Weight kips	VCG ft
	0.50	24.80	0.25
	1.00	49.60	0.50
	1.50	74.39	0.75
	2.00	99.19	1.00
	2.50	123.99	1.25
	3.00	148.79	1.50
	3.50	173.58	1.75
	4.00	198.38	2.00
	4.50	223.18	2.25
	5.00	247.98	2.50
	5.50	272.78	2.75
	6.00	297.57	3.00
	6.50	322.37	3.25
	7.00	347.17	3.50
	7.50	371.97	3.75
	8.00	396.76	4.00
	8.50	421.56	4.25
	9.00	446.36	4.50
	9.50	4/1.16	4.75
	10.00	495.96	5.00
	10.50	520.75	5.25
	11.00	545.55	5.50
	12.00	570.35	5.75
	12.00	595.15	6.00
	12.00	614.74	6.20
	13.50	669 54	6.75
	14.00	694 34	7.00
	14.50	719 13	7.00
	15.00	743 93	7 50
	15.50	768 73	7.75
	16.00	793.53	8.00
	16.50	818.33	8.25
	17.00	843.12	8.50
	17.50	867.92	8.75
	18.00	892.72	9.00
	18.50	917.52	9.25
	19.00	942.31	9.50
	19.50	967.11	9.75
	20.00	991.91	10.00

COASTAL DRILLER PRELOAD TANK 3

LCG TCG	28.85 ft -23.35 ft		FSML 8765 ft-kips FSMT 4511 ft-kips
	Sounding	Weight	VCG
	ft	kips	ft
	0.50	25.18	0.25
	1.00	50.36	0.50
	1.50	75.53	0.75
	2.00	100.71	1.00
	2.50	125.89	1.25
	3.00	151.07	1.50
	3.50	176.25	1.75
	4.00	201.42	2.00
	4.50	226.60	2.25
	5.00	251.78	2.50
	5.50	276.96	2.75
	6.00	302.14	3.00
	6.50	327.31	3.25
	7.00	352.49	3.50
	7.50	377.67	3.75
	8.00	402.85	4.00
	8.50	428.03	4.25
	9.00	453.20	4.50
	9.50	478.38	4.75
	10.00	503.56	5.00
	10.50	528.74	5.25
	11.00	553.92	5.50
	11.50	579.09	5.75
	12.00	604.27	6.00
	12.50	629.45	6.25
	13.00	654.63	6.50
	13.50	679.81	6.75
	14.00	704.98	7.00
	14.50	730.16	7.25
	15.00	755.34	7.50
	15.50	780.52	7.75
	16.00	805.70	8.00
	16.50	830.87	8.25
	17.00	856.05	8.50
	19.00	881.23	8.75
	10.00	906.41	9.00
	10.00	931.59	9.25
	19.00	950.76	9.50
	20.00	1007 12	9.75
	20.00	1007.12	10.00

COASTAL DRILLER POTABLE WATER TANKS 4 OR 5

LCG 65.36 ft TCG – 14.22 ft		FSML 1707 ft-kips FSMT 1965 ft-kips
Sounding	Weight	VCG
ft	kips	ft
0.25	8.61	0.13
0.50	17.22	0.25
0.75	25.83	0.38
1.00	34.45	0.50
1.25	43.06	0.63
1.50	51.67	0.75
1.75	60.28	0.88
2.00	68.89	1.00
2.25	77.50	1.13
2.50	86.12	1.25
2.75	94.73	1.38
3.00	103.34	1.50
3.25	111.95	1.63
3.50	120.56	1.75
3.75	129.17	1.88
4.00	137.78	2.00
4.25	146.40	2.13
4.50	155.01	2.25
4.75	163.62	2.38
5.00	172.23	2.50

COASTAL DRILLER DRILL WATER TANK 6 OR 7

LCG	78.30 ft		FSML 4464 ft-kips
TCG	33.51 ft (Tar	nk 6)	FSMT 932 ft-kips
	-33.51 ft (Tank 7)		
	Sounding ft	Weight	VCG
		pe	
	0.25	8.35	0.13
	0.50	16.71	0.25
	0.75	25.06	0.38

0.20	0.35	0.13
0.50	16.71	0.25
0.75	25.06	0.38
1.00	33.42	0.50
1.25	41.77	0.63
1.50	50.12	0.75
1.75	58.48	0.88
2.00	66.83	1.00
2.25	75.19	1.13
2.50	83.54	1.25
2.75	91.89	1.38
3.00	100.25	1.50
3.25	108.60	1.63
3.50	116.96	1.75
3.75	125.31	1.88
4.00	133.66	2.00
4.25	142.02	2.13
4.50	150.37	2.25
4.75	158.73	2.38
5.00	167.08	2.50

COASTAL DRILLER PRELOAD TANK 8

LCG TCG	69.17 ft 44.46 ft		FSML 2779 ft-kips FSMT 900 ft-kips
	Sounding	Weight	VCG
	ft	kips	ft
	0.50	14.53	0.25
	1.00	29.05	0.50
	1.50	43.58	0.75
	2.00	58.11	1.00
	2.50	72.63	1.25
	3.00	87.16	1.50
	3.50	101.68	1.75
	4.00	116.21	2.00
	4.50	130.74	2.25
	5.00	145.26	2.50
	5.50	159.79	2.75
	6.00	174.32	3.00
	6.50	188.84	3.25
	7.00	203.37	3.50
	7.50	217.89	3.75
	8.00	232.42	4.00
	8.50	246.95	4.25
	9.00	261.47	4.50
	9.50	276.00	4.75
	10.00	290.53	5.00
	10.50	305.05	5.25
	11.00	319.58	5.50
	11.50	334.10	5.75
	12.00	348.63	6.00
	12.50	363.16	6.25
	13.00	377.68	6.50
	13.50	392.21	6.75
	14.00	406.74	7.00
	14.50	421.26	7.25
	15.00	435.79	7.50
	15.50	450.31	7.75
	16.00	464.84	8.00
	16.50	479.37	8.25
	17.00	493.89	8.50
	17.50	508.42	8.75
	18.00	522.95	9.00
	18.50	537.47	9.25
	19.00	552.00	9.50
	19.50	500.52	9.75
	20.00	581.05	10.00

COASTAL DRILLER PRELOAD TANK 9

LCG TCG	68.17 ft 43.71 ft		FSML 3266 ft-kips FSMT 1168 ft-kips
	Sounding ft	Weight kips	VCG ft
	0.50	15 51	0.25
	1.00	31.03	0.50
	1.50	46.54	0.75
	2.00	62.06	1.00
	2.50	77.57	1.25
	3.00	93.08	1.50
	3.50	108.60	1.75
	4.00	124.11	2 00
	4.50	139.62	2.25
	5.00	155.14	2.50
	5.50	170.65	2.75
	6.00	186.17	3.00
	6.50	201.68	3.25
	7.00	217.19	3.50
	7.50	232.71	3.75
	8.00	248.22	4.00
	8.50	263.73	4.25
	9.00	279.25	4.50
	9.50	294.76	4.75
	10.00	310.28	5.00
	10.50	325.79	5.25
	11.00	341.30	5.50
	11.50	356.82	5.75
	12.00	372.33	6.00
	12.50	387.84	6.25
	13.00	403.36	6.50
	13.50	418.87	6.75
	14.00	434.39	7.00
	14.50	449.90	7.25
	15.00	465.41	7.50
	10.00	480.93	7.75
	16.00	496.44	8.00
	17.00	511.95	8.25
	17.00	527.47	8.50
	18.00	542.98	8.75
	18.50	574.01	9.00
	19.00	574.01	9.25
	19.50	605.04	9.50
	20.00	620.55	9.75

COASTAL DRILLER DRILL WATER TANK 10 OR 11

LCG TCG	85.30 ft 12.08 ft (Tank 10) - 12.08 ft (Tank 11)		FSML 725 ft-kips FSMT 1345 ft-kips	
	Sounding ft	Weight kips	VCG ft	
	0.25	6.54	0.13	
	0.50	13.07	0.25	
	0.75	19.61	0.38	
	1.00	26.15	0.50	
	1.25	32.69	0.63	
	1.50	39.22	0.75	
	1.75	45.76	0.88	
	2.00	52.30	1.00	
	2.25	58.83	1.13	
	2.50	65.37	1.25	
	2.75	71.91	1.38	
	3.00	78.44	1.50	
	3.25	84.94	1.63	
	3.50	91.52	1.75	
	3.75	98.06	1.88	
	4.00	104.59	2.00	
	4.25	111.13	2.13	
	4.50	117.67	2.25	
	4.75	124.20	2.38	
	5.00	130.74	2.50	

COASTAL DRILLER DIESEL FUEL TANK 13

LCG TCG	105.94 ft -41.41 ft		FSML 404 ft-kips FSMT 1034 ft-kips
	Sounding ft	Weight kips	VCG ft
	0.05		0.10
	0.25	4.47	0.13
	0.50	8.93	0.25
	0.75	13.40	0.38
	1.00	17.86	0.50
	1.25	22.33	0.63
	1.50	26.79	0.75
	1.75	31.26	0.88
	2.00	35.72	1.00
	2.25	40.19	1.13
	2.50	44.65	1.25
	2.75	49.12	1.38
	3.00	53.58	1.50
	3.25	58.05	1.63
	3.50	62.51	1.75
	3.75	66.98	1.88
	4.00	71.44	2.00
	4.25	75.91	2.13
	4.50	80.37	2.25
	4.75	84.84	2.38
	5.00	89.30	2.50

COASTAL DRILLER DIESEL FUEL TANK 14

LCG TCG	104.12 ft 39.16 ft		FSML 674 ft-kips FSMT 1492 ft-kips
	Sounding	Weight	VCG
	ft	kips	ft
	0.25	6.10	0.13
	0.50	12.20	0.25
	0.75	18.30	0.38
	1.00	24.40	0.50
	1.25	30.50	0.63
	1.50	36.60	0.75
	1.75	42.70	0.88
	2.00	48.80	1.00
	2.25	54.90	1.13
	2.50	61.00	1.25
	2.75	67.09	1.38
	3.00	73.19	1.50
	3.25	79.29	1.63
	3.50	85.39	1.75
	3.75	91.49	1.88
	4.00	97.59	2.00
	4.25	103.69	2.13
	4.50	109.79	2.25
	4.75	115.89	2.38
	5.00	121.99	2.50
COASTAL DRILLER PRELOAD TANK 15 OR 16

LCG TCG	103.66 ft –59.26 ft (Tank 15) 59.26 ft (Tank 16)		FSML 3548 ft-kips FSMT 1239 ft-kips	
	Sounding ft	Weight kips	VCG ft	
	0.50	15.96	0.25	
	1.00	31.91	0.50	
	1.50	47.87	0.75	
	2.00	63.83	1.00	
	2.50	79.79	1.25	
	3.00	95.74	1.50	
	3.50	111.70	1.75	
	4.00	127.66	2.00	
	4.50	143.61	2.25	
	5.00	159.57	2.50	
	5.50	175.53	2.75	
	6.00	191.48	3.00	
	6.50	207.44	3.25	
	7.00	223.40	3.50	
	7.50	239.36	3.75	
	8.00	255.31	4.00	
	8.50	271.27	4.25	
	9.00	287.23	4.50	
	9.50	303.18	4.75	
	10.00	319.14	5.00	
	10.50	335.10	5.25	
	11.00	351.05	5.50	
	11.50	367.01	5.75	
	12.00	382.97	6.00	
	12.50	398.93	6.25	
	13.00	414.88	6.50	

430.84

446.80

462.75

478.71

494.67

510.62

526.58

542.54

558.50

574.45

590.41

606.37

622.32

638.28

13.50

14.00

14.50

15.00

15.50

16.00

16.50

17.00

17.50

18.00

18.50

19.00

19.50

20.00

6.75

7.00

7.25

7.50

7.75

8.00

8.25

8.50

8.75

9.00

9.25

9.50

9.75

10.00

COASTAL DRILLER DRILL WATER TANK 17

LCG 126.16 ft TCG -13.00 ft	FSML 2659 ft-kips FSMT 2464 ft-kips		
Sounding ft	Weight kips	VCG ft	
0.25	10.62	0.13	
0.50	21.25	0.25	
0.75	31.87	0.38	
1.00	42.49	0.50	
1.25	53.11	0.63	
1.50	63.74	0.75	
1.75	74.36	0.88	
2.00	84.98	1.00	
2.25	95.60	1.13	
2.50	106.23	1.25	
2.75	116.85	1.38	
3.00	127.47	1.50	
3.25	138.09	1.63	
3.50	148.72	1.75	
3.75	159.34	1.88	
4.00	169.96	2.00	
4.25	180.58	2.13	
4.50	191.21	2.25	
4.75	201.83	2.38	
5.00	212.45	2.50	

COASTAL DRILLER DRILL WATER TANK 18

LCG 126.91 ft TCG 12.17 ft		FSML 2340 ft-kips FSMT 2090 ft-kips	
Sounding ft	Weight kips	VCG ft	
0.25	9.81	0.13	
0.50	19.61	0.25	
0.75	29.42	0.38	
1.00	39.22	0.50	
1.25	49.03	0.63	
1.50	58.83	0.75	
1.75	68.64	0.88	
2.00	78.44	1.00	
2.25	88.25	1.13	
2.50	98.06	1.25	
2.75	107.86	1.38	
3.00	117.67	1.50	
3.25	127.47	1.63	
3.50	137.28	1.75	
3.75	147.08	1.88	
4.00	156.89	2.00	
4.25	166.69	2.13	
4.50	176.50	2.25	
4.75	186.30	2.38	
5.00	196.11	2.50	

COASTAL DRILLER DIESEL FUEL TANK 19

LCG 126.37 ft TCG -42.69 ft		FSML 2870 ft-kips FSMT 4485 ft-kips		
Sounding	Weight	VCG		
π	KIPS	π		
0.25	11.68	0.13		
0.50	23.36	0.25		
0.75	35.04	0.38		
1.00	46.72	0.50		
1.25	58.40	0.63		
1.50	70.08	0.75		
1.75	81.76	0.88		
2.00	93.44	1.00		
2.25	105.12	1.13		
2.50	116.80	1.25		
2.75	128.48	1.38		
3.00	140.16	1.50		
3.25	151.84	1.63		
3.50	163.52	1.75		
3.75	175.20	1.88		
4.00	186.88	2.00		
4.25	198.56	2.13		
4.50	210.24	2.25		
4.75	221.92	2.38		
5.00	233.60	2.50		

COASTAL DRILLER DIESEL FUEL TANK 20

LCG 126.71 ft TCG 41.20 ft		FSML 1774 ft-kips FSMT 3474 ft-kips	
Sounding	Weight	VCG	
	Rips	π	
0.25	8.67	0.13	
0.50	17.35	0.25	
0.75	26.02	0.38	
1.00	34.70	0.50	
1.25	43.37	0.63	
1.50	52.05	0.75	
1.75	60.72	0.88	
2.00	69.40	1.00	
2.25	78.07	1.13	
2.50	86.75	1.25	
2.75	95.42	1.38	
3.00	104.09	1.50	
3.25	112.77	1.63	
3.50	121.44	1.75	
3.75	130.12	1.88	
4.00	138.79	2.00	
4.25	147.47	2.13	
4.50	156.14	2.25	
4.75	164.82	2.38	
5.00	173.49	2.50	

6-17

COASTAL DRILLER PRELOAD TANK 21A

LCG 141.75 ft TCG -74.95 ft		FSML 7328 ft-kips FSMT 2413 ft-kips	
Sounding ft	Weight kips	VCG ft	
0.50	17 67	0.25	
1.00	35.34	0.50	
1.50	53.01	0.75	
2.00	70.68	1.00	
2.50	88.35	1.25	
3.00	106.02	1.50	
3.50	123.69	1.75	
4.00	141.36	2.00	
4.50	159.03	2.25	
5.00	176.70	2.50	
5.50	194.37	2.75	
6.00	212.04	3.00	
6.50	229.71	3.25	
7.00	247.38	3.50	
7.50	265.05	3.75	
8.00	282.72	4.00	
8.50	300.39	4.25	
9.00	318.06	4.50	
9.50	335.73	4.75	
10.00	353.40	5.25	
11.00	299 74	5.50	
11.00	406 41	5.75	
12.00	424 08	6.00	
12.00	441.75	6.25	
13.00	459.42	6.50	
13.50	477.09	6.75	
14.00	494.76	7.00	
14.50	512.43	7.25	
15.00	530.10	7.50	
15.50	547.77	7.75	
16.00	565.44	8.00	
16.50	583.11	8.25	
17.00	600.78	8.50	
17.50	618.45	8.75	
18.00	636.12	9.00	
18.50	653.79	9.25	
19.00	6/1.46	9.50	
19.50	689.13	9./5	
20.00	706.80	10.00	

COASTAL DRILLER PRELOAD TANK 21B

LCG TCG	184.06 ft 65.02 ft		FSML 1069 ft-kips FSMT 3950 ft-kips	
Sound ft	ling	Weight kips	VCG ft	
0.5	50	13.98	0.25	
1.0	00	27.96	0.50	
1.5	50	41.94	0.75	
2.0	00	55.92	1.00	
2.5	50	69.90	1.25	
3.0	00	83.88	1.50	
3.5	50	97.86	1.75	
4.0	00	111.84	2.00	
4.5	50	125.82	2.25	
5.0	00	139.80	2.50	
5.5	50	153.78	2.75	
6.0	00	167.76	3.00	
6.5	50	181.74	3.25	
7.0	00	195.72	3.50	
7.5	50	209.70	3.75	
8.0	00	223.68	4.00	
8.3	50	237.66	4.25	
9.0	50	251.64	4.50	
9.0	50	265.62	4.75	
10.0	50	279.60	5.00	
11.	30	293.38	5.25	
11.0	50	201.50	5.50	
120	0	335 52	6.00	
12.0	50	349 50	6.25	
130	00	363.49	6.50	
13.	50	377 46	6.75	
14 (00	391 44	7.00	
14	50	405 42	7.25	
15.0	00	419 40	7.50	
15.	50	433.38	7.75	
16.00		447.36	8.00	
16.	50	461.34	8.25	
17.0	00	475.32	8.50	
17.	50	489.30	8.75	
18.0	00	503.28	9.00	
18.5	50	517.26	9.25	
19.0	00	531.24	9.50	
19.5	50	545.22	9.75	
20.0	00	559.20	10.00	

6-19

COASTAL DRILLER PRELOAD TANK 22A

LCG 141.65 ft TCG 74.98 ft		FSML 7348 ft-kips FSMT 2415 ft-kips	
Sounding ft	Weight kips	VCG ft	
0.50	10.00	0.05	
0.50	18.02	0.25	
1.00	36.05	0.50	
1.50	54.07	0.75	
2.00	72.09	1.00	
2.50	90.12	1.25	
3.00	108.14	1.50	
3.50	126.16	1.75	
4.00	144.19	2.00	
4.50	162.21	2.25	
5.00	180.24	2.50	
5.50	198.26	2.75	
6.00	216.28	3.00	
6.50	234.31	3.25	
7.00	252.33	3.50	
7.50	270.35	3.75	
8.00	288.38	4.00	
8.50	306.40	4.25	
9.00	324.42	4.50	
9.50	342.45	4.75	
10.00	360.47	5.00	
10.50	378.49	5.25	
11.00	396.52	5.50	
11.50	414.54	5.75	
12.00	432.56	6.00	
12.50	450.59	6.25	
13.00	468.61	6.50	
13.50	486.63	6.75	
14.00	504.66	7.00	
14.50	522.68	7.25	
15.00	540./1	7.50	
15.50	558.73	1.75	
16.00	576.75	8.00	
16.50	594.78	8.25	
17.00	612.80	8.50	
17.50	630.82	8.75	
18.00	648.85	9.00	
18.50	666.87	9.25	
19.00	684.89	9.50	
19.50	702.92	9.75	
20.00	720.94	10.00	

COASTAL DRILLER PRELOAD TANK 22B

LCG 184.05 ft TCG See right column		FSML 1069 ft-kips FSMT 3950 ft-kips	
Sounding ft	Weight kips	VCG ft	TCG ft
0.50	13.16	0.25	65.02
1.00	26.32	0.50	65.02
1.50	39.48	0.75	65.11
2.00	52.64	1.00	65.28
2.50	65.80	1.25	65.39
3.00	78.96	1.50	65.46
3.50	92.12	1.75	65.51
4.00	105.28	2.00	65.55
4.50	118.44	2.25	65.58
5.00	131.61	2.50	65.60
5.50	144.77	2.75	65.62
6.00	157.93	3.00	65.64
6.50	171.09	3.25	65.65
7.00	184.25	3.50	65.67
7.50	197.41	3.75	65.68
8.00	210.57	4.00	65.69
8.50	223.73	4.25	65.69
9.00	236.89	4.50	65.70
9.50	250.05	4.75	65.71
10.00	263.21	5.00	65.71
10.50	276.37	5.25	65.72
11.00	289.53	5.50	65.72
11.50	302.69	5.75	65.73
12.00	315.85	6.00	65.73
12.50	329.01	6.25	65.74
13.00	342.17	6.50	65.74
13.50	355.33	6.75	65.75
14.00	368.49	7.00	65.75
14.50	381.65	7.25	65.75
15.00	394.82	7.50	65.75
15.50	407.98	7.75	65.75
16.00	421.14	8.00	65.76
16.50	434.30	8.25	65.76
17.00	447.46	8.50	65.76
17.50	460.62	8.75	65.76
18.00	473.78	9.00	65.76
18.50	486.94	9.25	65.77
19.00	500.10	9.50	65.77
19.50	513.26	9.75	65.77
20.00	526.42	10.00	65.77

COASTAL DRILLER DRILL WATER TANK 23 OR 24

LCG	156.00	ft	FSML 4708 ft-kips
TCG	-13.00	ft (Tank 23)	FSMT 2982 ft-kips
	13.00	ft (Tank 24)	
Sound	ding	Weight	VCG
ft		kips	ft

11	KIPS	п
0.25	12.85	0.13
0.50	25.71	0.25
0.75	38.56	0.38
1.00	51.41	0.50
1.25	64.27	0.63
1.50	77.12	0.75
1.75	89.97	0.88
2.00	102.83	1.00
2.25	115.68	1.13
2.50	128.54	1.25
2.75	141.39	1.38
3.00	154.24	1.50
3.25	167.10	1.63
3.50	179.95	1.75
3.75	192.80	1.88
4.00	205.66	2.00
4.25	218.51	2.13
4.50	231.36	2.25
4.75	244.22	2.38
5.00	257.07	2.50

COASTAL DRILLER DRILL WATER TANK 25 OR 26

LCG	154.62 ft	FSML:	3045 ft-kips
TCG	-34.00 ft (Tank 25)	FSMT	777 ft-kips
	34.00 ft (Tank 26)		

Sounding ft	Weight kips	VCG ft
0.25	7.59	0.13
0.50	15.18	0.25
0.75	22.77	0.38
1.00	30.36	0.50
1.25	37.95	0.63
1.50	45.54	0.75
1.75	53.13	0.88
2.00	60.72	1.00
2.25	68.31	1.13
2.50	75.90	1.25
2.75	83.49	1.38
3.00	91.08	1.50
3.25	98.67	1.63
3.50	106.26	1.75
3.75	113.85	1.88
4.00	121.44	2.00
4.25	129.03	2.13
4.50	136.62	2.25
4.75	144.21	2.38
5.00	151.80	2.50

COASTAL DRILLER PRELOAD TANK 28

LCG TCG	188.86 ft 36.10 ft		FSML 3966 ft-kips FSMT 1600 ft-kips
	Sounding ft	Weight kips	VCG ft
	0.50	21.28	0.25
	1.00	42.55	0.50
	1.50	63.83	0.75
	2.00	85.11	1.00
	2.50	106.38	1.25
	3.00	127.66	1.50
	3.50	148.94	1.75
	4.00	170.21	2.00
	4.50	191.49	2.25
	5.00	212.77	2.50
	5.50	234.04	2.75
	6.00	255.32	3.00
	6.50	276.60	3.25
	7.00	297.87	3.50
	7.50	319.15	3.75
	8.00	340.43	4.00
	8.50	361.70	4.25
	9.00	382.98	4.50
	9.50	404.26	4.75
	10.00	425.54	5.00
	11.00	440.01	5.20
	11.00	400.09	5.50
	12.00	409.37	5.75
	12.00	531 02	6.00
	12.00	553 20	6.50
	13.50	574 47	6.75
	14.00	595 75	7.00
	14.50	617.03	7.25
	15.00	638.30	7.50
	15.50	659.58	7.75
	16.00	680.86	8.00
	16.50	702.13	8.25
	17.00	723.41	8.50
	17.50	744.69	8.75
	18.00	765.96	9.00
	18.50	787.24	9.25
	19.00	808.52	9.50
	19.50	829.79	9.75
	20.00	851.07	10.00

6-24

COASTAL DRILLER PRELOAD TANK 29

LCG 188.79 TCG -36.28	9 ft 3 ft	FSML 7328 ft-kips FSMT 2413 ft-kips
Sounding	Weight	VCG
ft	kips	ft
0.50	21.66	0.25
1.00	43.31	0.25
1.50	64 97	0.30
2.00	86.63	1.00
2.50	108 29	1.25
3.00	129.94	1.50
3.50	151.60	1.75
4.00	173.26	2.00
4.50	194.91	2.25
5.00	216.57	2.50
5.50	238.23	2.75
6.00	259.88	3.00
6.50	281.54	3.25
7.00	303.20	3.50
7.50	324.86	3.75
8.00	346.51	4.00
8.50	368.17	4.25
9.00	389.83	4.50
9.50	411.48	4.75
10.00	433.14	5.00
10.50	454.80	5.25
11.00	476.45	5.50
11.50	498.11	5.75
12.00	519.77	6.00
12.50	541.43	6.25
13.00	563.08	6.50
13.50	584.74	6.75
14.00	606.40	7.00
15.00	640 71	7.25
15.50	671 37	7.50
16.00	693.02	8.00
16.50	714 68	8.25
17.00	736.34	8.50
17.50	758.00	8.75
18.00	779.65	9.00
18.50	801.31	9.25
19.00	822.97	9.50
19.50	844.62	9.75
20.00	866.28	10.00

6-25

COASTAL DRILLER DIRTY OIL TANK 31

LCG 117.16 TCG 23.00	ft ft	FSML FSMT	20 ft-kips 8 ft-kips
Sounding ft	Weight kips	V	CG It
0.25	0.73	(0.13
0.50	1.46	(0.25
0.75	2.20	(0.38
1.00	2.93	(0.50
1.25	3.66	(0.63
1.50	4.39	(0.75
1.75	5.12	(0.88
2.00	5.86	-	.00
2.25	6.59		1.13
2.50	7.32	1	.25
2.75	8.05	i.	.38
3.00	8.78	-	1.50
3.25	9.52		.63
3.50	10.25	1	.75
3.75	10.98	1	.88
4.00	11.71	2	2.00
4.25	12.44	2	2.13
4.50	13.18	2	2.25
4.75	13.91	2	2.38
5.00	14.64	2	2.50

COASTAL DRILLER SKIM TANK

LCG TCG	185.00 ft 54.00 ft		FSML FSMT	1 ft-kip 1 ft-kip
	Sounding ft	Weight kips	VCG ft	
	0.50	0.88	0.25	
	1.00	1.76	0.50	
	1.50	2.65	0.75	
	2.00	3.53	1.00	
	2.50	4.41	1.25	
	3.00	5.29	1.50	
	3.50	6.18	1.75	
	4.00	7.06	2.00	
	4.50	7.94	2.25	
	5.00	8.82	2.50	
	5.50	9.71	2.75	
	6.00	10.59	3.00	
	6.50	11.47	3.25	
	7.00	12.35	3.50	
	7.50	13.24	3.75	
	8.00	14.12	4.00	
	0.00	15.00	4.25	
	9.50	16 77	4.50	
	10.00	17.65	5.00	
	10.50	18.53	5.00	
	11.00	19.41	5.50	
	11.50	20.30	5.75	
	12.00	21.18	6.00	
	12.50	22.06	6.25	
	13.00	22.94	6.50	
	13.50	23.83	6.75	
	14.00	24.71	7.00	
	14.50	25.59	7.25	
	15.00	26.47	7.50	
	15.50	27.35	7.75	
	16.00	28.24	8.00	
	16.50	29.12	8.25	
	17.00	30.00	8.50	
	17.50	30.88	8.75	
	18.00	31.77	9.00	
	18.50	32.65	9.25	
	18.63	32.87	9.31	

COASTAL DRILLER MUDPIT 1S

LCG 103.66 ft TCG 19.50 ft	FSMI FSM ⁻	- 633 ft-kips T 328 ft-kips
Sounding	Weight	VCG
π	kips	ft
0.25	5.79	5.13
0.50	11.58	5.25
0.75	17.37	5.38
1.00	23.17	5.50
1.25	28.96	5.63
1.50	34.75	5.75
1.75	40.54	5.88
2.00	46.33	6.00
2.25	52.12	6.13
2.50	57.92	6.25
2.75	63.71	6.38
3.00	69.50	6.50
3.25	75.29	6.63
3.50	81.08	6.75
3.75	86.87	6.88
4.00	92.67	7.00
4.25	98.46	7.13
4.50	104.25	7.25
4.75	110.04	7.38
5.00	115.83	7.50
5.25	121.62	7.63
5.50	127.41	7.75
5.75	133.21	7.88
6.00	139.00	8.00
6.25	144.79	8.13
6.50	150.58	8.25
6.75	156.37	8.38
7.00	162.16	8.50
7.25	167.96	8.63
7.50	173.75	8.75
1.75	1/9.54	8.88
8.00	185.33	9.00

COASTAL DRILLER MUDPIT 2S

LCG 104.67 ft TCG 5.85 ft	FSML 481 ft-kips FSMT 263 ft-kips	
Sounding ft	Weight kips	VCG ft
0.25	4.94	5.13
0.50	9.88	5.25
0.75	14.82	5.38
1.00	19.76	5.50
1.25	24.70	5.63
1.50	29.64	5.75
1.75	34.58	5.88
2.00	39.53	6.00
2.25	44.47	6.13
2.50	49.41	6.25
2.75	54.35	6.38
3.00	59.29	6.50
3.25	64.23	6.63
3.50	69.17	6.75
3.75	74.11	6.88
4.00	79.05	7.00
4.25	83.99	7.13
4.50	88.93	7.25
4.75	93.87	7.38
5.00	98.81	7.50
5.25	103.75	7.63
5.50	108.69	7.75
5.75	113.63	7.88
6.00	118.58	8.00
6.25	123.52	8.13
6.50	128.46	8.25
6.75	133.40	8.38
7.00	138.34	8.50
7.25	143.28	8.63
7.50	148.22	8.75
7.75	153.16	8.88
8.00	158.10	9.00

COASTAL DRILLER MUDPIT 3P

TCG	103.66 ft - 6.50 ft	FSML 633 ft-kips FSMT 328 ft-kips
Sounding ft	Weight kips	VCG ft
0.25	5.79	5 13
0.50	11.58	5.25
0.75	17.37	5.38
1.00	23.17	5.50
1.25	28.96	5.63
1.50	34.75	5.75
1.75	40.54	5.88
2.00	46.33	6.00
2.25	52.12	6.13
2.50	57.92	6.25
2.75	63.71	6.38
3.00	69.50	6.50
3.25	75.29	6.63
3.50	81.08	6.75
3.75	86.87	6.88
4.00	92.67	7.00
4.25	98.46	7.13
4.50	104.25	7.25
4.75	110.04	7.38
5.00	115.83	7.50
5.25	121.62	7.63
5.50	127.41	7.75
5.75	133.21	7.88
6.00	139.00	8.00
6.25	144.79	8.13
6.50	150.58	8.25
6.75	156.37	8.38
7.00	162.16	8.50
7.25	167.96	8.63
7.50	173.75	8.75
7.75	179.54	8.88
8.00	185.33	9.00

COASTAL DRILLER MUDPIT 4P

LCG 103.66 ft TCG – 19.50 ft	FSN FSN	AL 633 ft-kips AT 328 ft-kips
Sounding ft	Weight kips	VCG ft
0.25	5.79	5 13
0.50	11.58	5.25
0.75	17.37	5.38
1.00	23.17	5.50
1.25	28.96	5.63
1.50	34.75	5.75
1.75	40.54	5.88
2.00	46.33	6.00
2.25	52.12	6.13
2.50	57.92	6.25
2.75	63.71	6.38
3.00	69.50	6.50
3.25	75.29	6.63
3.50	81.08	6.75
3.75	86.87	6.88
4.00	92.67	7.00
4.25	98.46	7.13
4.50	104.25	7.25
4.75	110.04	7.38
5.00	115.83	7.50
5.25	121.62	7.63
5.50	127.41	7.75
5.75	133.21	7.88
6.00	139.00	8.00
6.25	144.79	8.13
6.50	150.58	8.25
6.75	156.37	8.38
7.00	162.16	8.50
7.25	167.96	8.63
7.50	173.75	8.75
7.75	179.54	8.88
8.00	185.33	9.00

COASTAL DRILLER SLUGGING PIT

LCG TCG	97.76 ft 10.25 ft		FSML 11 ft-kips FSMT 8 ft-kips
	Sounding ft	Weight kips	VCG ft
	0.25	0.85	5.13
	0.50	1.70	5.25
	0.75	2.55	5.38
	1.00	3.40	5.50
	1.25	4.25	5.63
	1.50	5.11	5.75
	1.75	5.96	5.88
	2.00	6.81	6.00
	2.25	7.66	6.13
	2.50	8.51	6.25
	2.75	9.36	6.38
	3.00	10.21	6.50
	3.25	11.06	6.63
	3.50	11.91	6.75
	3.75	12.76	6.88
	4.00	13.62	7.00
	4.25	14.47	7.13
	4.50	15.32	7.25
	4.75	16.17	7.38
	5.00	17.02	7.50
	5.25	17.87	7.63
	5.50	18.72	7.75
	5.75	19.57	7.88
	6.00	20.42	8.00
	6.25	21.27	8.13
	6.50	22.12	8.25
	6.75	22.98	8.38
	7.00	23.83	8.50
	7.25	24.68	8.63
	7.50	25.53	8.75
	7.75	26.38	8.88
	8 00	27 23	9.00

INDEX

A

Abandonment, 3-11 Afloat, Changing Modes, 2-8 Afloat, Limits of Service, 5-21 Afloat Operations, 2-5 Afloat Preparations, 2-1 Afloat Recommendations, 2-7 Afloat, Storm Recomendations, 2-7 Afloat Stability, 4-4 Air Gap, 3-3, 3-9, 3-10 Allowable KG Curves, 5-6 Allowable Wind/Wave Charts, 3-5, 3-7, 5-2, 5-9 through 5-20

B

Basic Load, 1-6 Bilge Dewatering System, 2-11, 5-28 BM, 5-1 Bulk Capacities, 1-3

С

Cantilever Beams, 1-6 Cantilever Load Chart, 5-3, 5-22 Capacity, Bulk, 1-3 Capacity, Drilling Components, 1-8 Capacity, Elevating System, 1-8 Capacity, Elevating System, 1-8 Capacity, Liquid and Bulk, 1-3 Capacity, Tanks, 1-3 Centers of Gravity, 1-5, 1-6 Changes to Lightweight, 5-3, 5-23 Changing Modes, Afloat, 2-8 Classification, 1-1 Conductor Tension, 1-5

D

Deck Loads, Design, 1-3 Design Limits of Legs, Afloat, 5-2, 5-7 Dimensions, 1-2 Displacement, Load Line, 1-2 Draft, 2-8, 4-4, 4-6 Draft, Load Line, 1-2, 4-4 Draft Mark Locations, 1-2 Drilling Components, Capacity, 1-8 Drilling Loads, 1-4 Drilling Operations, 3-6

E

Elevated Load Capacity, 1-8 Elevated Operations, Instructions, 3-4 Elevated Operations, Preparations, 3-1 Elevated Operations, Skidding, 3-6 Elevated Operations, Storm, 3-8 Elevated Operations, Limits of Service, 3-9, 5-21 Emergency Procedures, Afloat, 2-8 Emergency Procedures, Afloat, 2-8 Emergency Procedures, Elevated, 3-10 Environmental Considerations, 1-3 Evacuation Procedures. 3-11

F

Field Transit, 2-5 Fixed Load, 1-4

F (Continued) Free Surface Correction, 4-5, 6-1 Free Surface Moments, 4-5, 6-1

Η

Heel, 4-6 Hull, Dimensions, 1-2 Hydrostatic Properties, 4-4, 5-1, 5-4

Ice, 1-3, 1-8 Inspections, 1-9

J

Jacking Operations, 3-2, 3-4 Jacking Preparation, 3-1, 3-2 Jetting Out, 2-4

K

KB, 5-1 KG, 4-5 KML, 4-4 KMT, 4-4 LCB, 4-4, 5-1 LCF, 5-1

L

Leg and Spud Can Weight, 1-6 Leg Reactions, 3-5, 4-7, 5-24 Leg Reactions, Elevated Limits, 3-5, 3-9. 5-21 Legs, Design Limits, Afloat, 2-6, 5-2, 5-7 Legs, Longitudinal Centers, 1-6 Legs, Transverse Centers, 1-6 Lightweight Amendment, 1-6, 5-23 Lightweight Weights, 1-5, 1-6 Limits, Going-On Location, 3-1, 5-8 Limits of Legs, Afloat, 2-6, 5-2, 5-7 Limits of Service, Afloat, 2-6 Limits of Service, Elevated, 3-9, 5-21 Liquid and Bulk Capacities, 1-3 List, 4-6 Load Form, 2-2, 4-1 Load Form Samples Drilling, 4-21 Elevated Severe Storm, 4-25 Preload, 4-17 Rig Move, 4-13 Load Line Displacement, 1-2, 4-4 Load Line Draft, 1-2, 4-4 Loads, Variable, 1-7 Lowering Hull, 2-3

M

Marine Growth, 1-9 Motions, Maximum for Going-On Location, 3-1, 5-2, 5-8

0

Offshore Installation Manager (OIM), 1-2 Operations, Afloat, 2-5 Operations, Elevated, 3-6

Ρ

Person-in-Charge, 1-2 Precision, 1-10 Preload, 1-4, 3-3 Preload Capacity, 1-7, 3-3 Preload Distribution, 4-8, 5-28 Preload, Maximum, 3-3 Preload, Minimum, 3-3 Preload Requirements, 1-7

R

Raising the Hull, 3-2, 3-4 Reference Planes, 1-9 Refloating the Unit, 2-3 Rotary Load, 1-5, 5-22

S

Safe Motion for Going on Location, 3-1, 5-2, 5-8 Sample Loading Conditions Drilling, 4-21 Elevated Severe Storm, 4-25 Preload, 4-17 Rig Move, 4-13 Setback, 1-5, 1-8 Severe Storm, 2-6, 2-7, 3-5, 3-8 Skidding the Drill Package, 3-6 Snow, 1-3, 1-8 Spud Can Reaction, 1-7 Stability Calculations, 4-1 Stability Criteria, 2-1 Stability Standards, Damaged, 2-1 Stability Standards, Intact, 2-1 Storm Recommendations, Afloat, 2-7 Substructure, 1-6

Т

Tank Capacity Table, 6-1, 6-2 Temperature, Design, 1-3 Tests, 1-9 Transit, 2-5 Trim, 4-6

U

Unexpected List or Trim, 2-8

V

Variable Load, 1-4, 1-7

W

Watertight Integrity, 2-1 Wind and Wave Drilling Charts, 5-9